

$$1. \quad i = C \frac{dv}{dt}$$

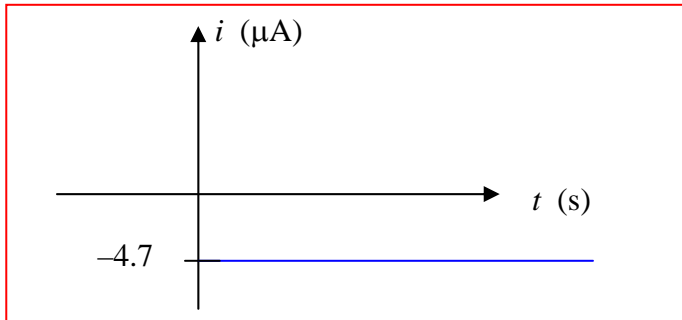
$$(a) \quad i = 0 \quad (\text{DC})$$

$$(b) \quad i = C \frac{dv}{dt} = -(10 \times 10^{-6})(115\sqrt{2})(120\pi) \sin 120\pi t = -613 \sin 120\pi t \text{ mA}$$

$$(c) \quad i = C \frac{dv}{dt} = -(10 \times 10^{-6})(4 \times 10^{-3})e^{-t} = -40e^{-t} \text{ nA}$$

$$2. \quad i = C \frac{dv}{dt}$$

$$v = \frac{6-0}{0-6}t + 6 = 6 - t, \text{ therefore } i = C \frac{dv}{dt} = -4.7 \times 10^{-6} \mu\text{A}$$



$$3. \quad i = C \frac{dv}{dt}$$

$$(a) \quad \frac{dv}{dt} = 30[e^{-t} - te^{-t}] \quad \text{therefore} \quad i = 10^{-3} \frac{dv}{dt} = 30(1-t)e^{-t} \text{ mA}$$

(b)

$$\frac{dv}{dt} = 4[-5e^{-5t} \sin 100t + 100e^{-5t} \cos 100t]$$

$$\text{therefore} \quad i = 10^{-3} \frac{dv}{dt} = 4e^{-5t} (100 \cos 100t - 5 \sin 100t) \text{ mA}$$

$$4. \quad W = \frac{1}{2}CV^2$$

$$(a) \quad \left(\frac{1}{2}\right)(2000 \times 10^{-6})1600 = \boxed{1.6 \text{ J}}$$

$$(b) \quad \left(\frac{1}{2}\right)(25 \times 10^{-3})(35)^2 = \boxed{15.3 \text{ J}}$$

$$(c) \quad \left(\frac{1}{2}\right)(10^{-4})(63)^2 = \boxed{198 \text{ mJ}}$$

$$(d) \quad \left(\frac{1}{2}\right)(2.2 \times 10^{-3})(2500) = \boxed{2.75 \text{ J}}$$

$$(e) \quad \left(\frac{1}{2}\right)(55)(2.5)^2 = \boxed{171.9 \text{ J}}$$

$$(f) \quad \left(\frac{1}{2}\right)(4.8 \times 10^{-3})(50)^2 = \boxed{6 \text{ J}}$$

$$5. \quad (a) \quad C = \frac{\epsilon A}{d} = \frac{8.854 \times 10^{-12} (78.54 \times 10^{-6})}{100 \times 10^{-6}} = 6.954 \text{ pF}$$

$$(b) \quad \text{Energy, } E = \frac{1}{2} CV^2 \therefore V = \sqrt{\frac{2E}{C}} = \sqrt{\frac{2(1 \times 10^{-3})}{6.954 \times 10^{-12}}} = 16.96 \text{ kV}$$

$$(c) \quad E = \frac{1}{2} CV^2 \therefore C = \frac{2E}{V^2} = \frac{2(2.5 \times 10^{-6})}{(100^2)} = 500 \text{ pF}$$

$$C = \frac{\epsilon A}{d} \therefore \epsilon = \frac{Cd}{A} = \frac{(500 \times 10^{-12})(100 \times 10^{-6})}{(78.54 \times 10^{-6})} = 636.62 \text{ pF} \cdot \text{m}^{-1}$$

$$\backslash \text{Relative permittivity: } \frac{\epsilon}{\epsilon_0} = \frac{636.62 \times 10^{-12}}{8.854 \times 10^{-12}} = 71.9$$

$$6. \quad (a) \quad \text{For } V_A = -1\text{V}, W = \sqrt{\frac{2K_s \epsilon_0}{qN} (V_{bi} - V_A)} = \sqrt{\frac{2(11.8)(8.854 \times 10^{-12})}{(1.6 \times 10^{-19})(1 \times 10^{24})}} (0.57 + 1)$$

$$= 45.281 \times 10^{-9} \text{ m}$$

$$C_j = \frac{11.8(8.854 \times 10^{-12})(1 \times 10^{-12})}{45.281 \times 10^{-9}} = \boxed{2.307 \text{ fF}}$$

$$(b) \quad \text{For } V_A = -5\text{V}, W = \sqrt{\frac{2K_s \epsilon_0}{qN} (V_{bi} - V_A)} = \sqrt{\frac{2(11.8)(8.854 \times 10^{-12})}{(1.6 \times 10^{-19})(1 \times 10^{24})}} (0.57 + 5)$$

$$= 85.289 \times 10^{-9} \text{ m}$$

$$C_j = \frac{11.8(8.854 \times 10^{-12})(1 \times 10^{-12})}{85.289 \times 10^{-9}} = \boxed{1.225 \text{ fF}}$$

$$(c) \quad \text{For } V_A = -10\text{V},$$

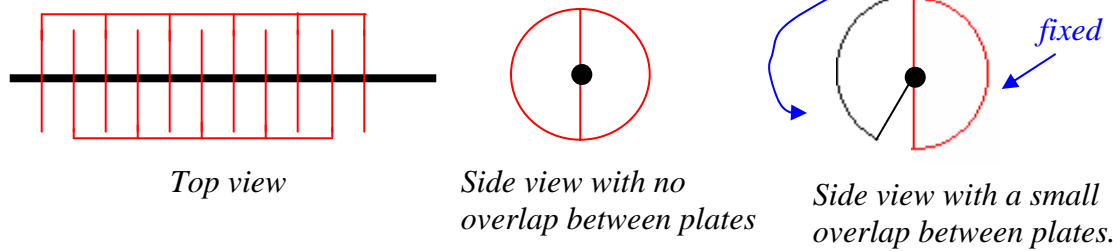
$$W = \sqrt{\frac{2K_s \epsilon_0}{qN} (V_{bi} - V_A)} = \sqrt{\frac{2(11.8)(8.854 \times 10^{-12})}{(1.6 \times 10^{-19})(1 \times 10^{24})}} (0.57 + 10)$$

$$= 117.491 \times 10^{-9} \text{ m}$$

$$C_j = \frac{11.8(8.854 \times 10^{-12})(1 \times 10^{-12})}{117.491 \times 10^{-9}} = \boxed{889.239 \text{ aF}}$$

7.

We require a capacitor that may be manually varied between 100 and 1000 pF by rotation of a knob. Let's choose an air dielectric for simplicity of construction, and a series of 11 half-plates:



Constructed as shown, the half-plates are in parallel, so that each of the 10 pairs must have a capacitance of  $1000/10 = 100$  pF when rotated such that they overlap completely. If we arbitrarily select an area of  $1 \text{ cm}^2$  for each half-plate, then the gap spacing between each plate is  $d = \epsilon A/C = (8.854 \times 10^{-14} \text{ F/cm})(1 \text{ cm}^2)/(100 \times 10^{-12} \text{ F}) = 0.8854 \text{ mm}$ . This is tight, but not impossible to achieve. The final step is to determine the amount of overlap which corresponds to 100 pF for the total capacitor structure. A capacitance of 100 pF is equal to 10% of the capacitance when all of the plate areas are aligned, so we need a pie-shaped wedge having an area of  $0.1 \text{ cm}^2$ . If the middle figure above corresponds to an angle of  $0^\circ$  and the case of perfect alignment (maximum capacitance) corresponds to an angle of  $180^\circ$ , we need to set out minimum angle to be  $18^\circ$ .

$$8. \quad (a) \quad \text{Energy stored} = \int_{t_0}^t v \cdot C \frac{dv}{dt} = C \int_0^{2 \times 10^{-3}} 3e^{-\frac{t}{5}} \cdot \left( -\frac{3}{5} e^{-\frac{t}{5}} \right) dt = \boxed{-1.080 \mu J}$$

$$(b) \quad V_{\max} = 3 \text{ V}$$

$$\text{Max. energy at } t=0, = \frac{1}{2} CV^2 = 1.35 \text{ mJ} \therefore 37\% E_{\max} = 499.5 \mu J$$

$$V \text{ at } 37\% E_{\max} = 1.825 \text{ V}$$

$$v(t) = 1.825 = 3e^{-\frac{t}{5}} \therefore t = 2.486 \text{ s} \Rightarrow \boxed{2 \text{ s}}$$

$$(c) \quad i = C \frac{dv}{dt} = 300 \times 10^{-6} \left( -\frac{3}{5} e^{-\frac{1.2}{5}} \right) = \boxed{-141.593 \mu A}$$

$$(d) \quad P = vi = 2.011 \left( -120.658 \times 10^{-6} \right) = \boxed{-242.6 \mu W}$$



9. (a) 
$$v = \frac{1}{C} \cdot \frac{\pi}{2} (1 \times 10^{-3})^2 = \frac{1}{47 \times 10^{-6}} \cdot \frac{(3.14159)}{2} (1 \times 10^{-3})^2 = 33.421 \text{ mV}$$
- (b) 
$$v = \frac{1}{C} \cdot \left( \frac{\pi}{2} (1 \times 10^{-3})^2 + 0 \right) = \frac{1}{47 \times 10^{-6}} \cdot \frac{(3.14159)}{2} (1 \times 10^{-3})^2 = 33.421 \text{ mV}$$
- (c) 
$$v = \frac{1}{C} \cdot \left( \frac{\pi}{2} (1 \times 10^{-3})^2 + \frac{\pi}{4} (1 \times 10^{-3})^2 \right) = \frac{1}{47 \times 10^{-6}} \cdot \left( \frac{3\pi}{4} (1 \times 10^{-3})^2 \right) = 50.132 \text{ mV}$$

$$10. \quad V = \frac{1}{C} \int_0^{200ms} i dt = \frac{1}{C} \left[ \left( -\frac{7 \times 10^{-3}}{\pi} \cos \pi t \right) \right]_0^{200ms} = \frac{0.426}{C}$$

$$E = \frac{1}{2} CV^2 = 3 \times 10^{-6} = \frac{181.086 \times 10^{-9}}{2C} \therefore C = \frac{181.086 \times 10^{-9}}{2(3 \times 10^{-6})} = \boxed{30181 \mu F}$$

11.

$$(a) \quad c = 0.2 \mu\text{F}, v_c = 5 + 3 \cos^2 200t \text{V}; \therefore i_c = 0.2 \times 10^{-6} (3) (-2) 200 \sin 200t \cos 200t$$

$$\therefore i_c = -0.12 \sin 400t \text{mA}$$

$$(b) \quad w_c = \frac{1}{2} c v_c^2 = \frac{1}{2} \times 2 \times 10^{-7} (5 + 3 \cos^2 200t)^2 \therefore w_{c \max} = 10^{-7} \times 64 = 6.4 \mu\text{J}$$

$$(c) \quad v_c = \frac{1}{0.2} \times 10^6 \int_0^t 8e^{-100t} \times 10^{-3} dt = 10^3 \times 40(-0.01)(e^{-100t} - 1) = 400(1 - e^{-100t}) \text{V}$$

$$(d) \quad v_c = 500 - 400e^{-100t} \text{V}$$

12.  $v_c(0) = 250\text{V}$ ,  $c = 2\text{mF}$  (a)  $v_c(0.1) = 250 + 500 \int_0^{0.1} 5 dt$   
 $\therefore v_c(0.1) = 500\text{V}; v_c(0.2) = 500 \int_{0.1}^{0.2} 10 dt = 1000\text{V}$   
 $\therefore v_c(0.6) = 1750\text{V}, v_c(0.9) = 2000\text{V}$   
 $\therefore 0.9 < t < 1: v_c = 2000 + 500 \int_{0.9}^t 10 dt = 2000 + 5000(t - 0.9)$   
 $\therefore v_c = 2100 = 2000 + 5000(t_2 - 0.9) \therefore t_2 = 0.92 \therefore 0.9 < t < 0.92\text{s}$

13.

$$(a) \quad w_c = \frac{1}{2} C v^2 = \frac{1}{2} \times 10^{-6} v^2 = 2 \times 10^{-2} e^{-1000t} \therefore v = \pm 200 e^{-500t} \text{ V}$$

$$i = C v' = 10^{-6} (\pm 200) (-500) e^{-500t} = \mp 0.1 e^{-500t}$$

$$\therefore R = \frac{-v}{i} = \frac{200}{0.1} = 2k\Omega$$

$$(b) \quad P_R = i^2 R = 0.01 \times 2000 e^{-1000t} = 20 e^{-1000t} \text{ W}$$

$$\therefore W_R = \int_0^{\infty} 20 e^{-1000t} dt = -0.02 e^{-1000t} \Big|_0^{\infty} = 0.02 \text{ J}$$

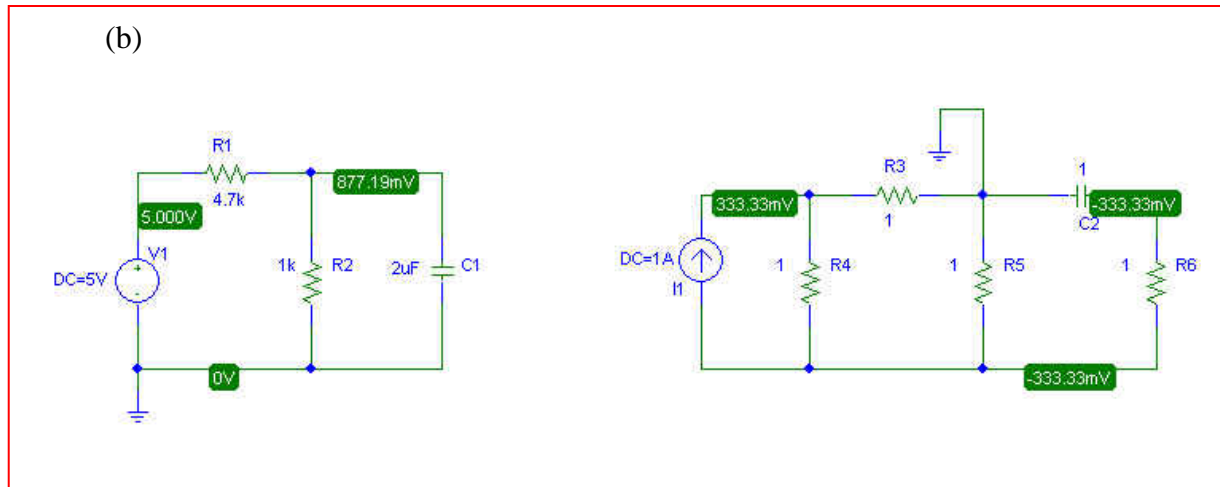
14. (a) Left circuit:

$$\text{By Voltage division, } V_C = \frac{1k}{4.7k + 1k}(5) = 0.877V$$

Right circuit:

$$V_1 = 1(1//2) = \frac{2}{3}V$$

$$\text{By Voltage Division, } V_2 = \frac{1}{3}V \therefore V_C = -\frac{1}{3}V$$



15.  $v = L \frac{di}{dt}$

(a)  $v = 0$  since  $i = \text{constant (DC)}$

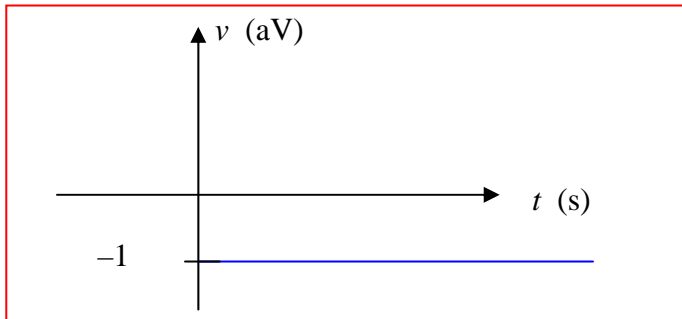
(b)  $v = -10^{-8} (115\sqrt{2})(120\pi) \sin 120\pi t = -613 \sin 120\pi t \text{ } \mu\text{V}$

(c)  $v = -10^{-8} (115\sqrt{2})(24 \times 10^{-3}) e^{-6t} = -240 e^{-6t} \text{ pV}$

16.  $v = L \frac{di}{dt}$

$$i = \left[ \frac{(6-0) \times 10^{-9}}{(0-6) \times 10^{-3}} \right] t + 6 \times 10^{-9} = 6 \times 10^{-9} - 10^{-6} t, \text{ therefore}$$

$$v = L \frac{di}{dt} = -(10^{-12})(10^{-6}) = -10^{-18} \text{ V} = -1 \text{ aV}$$





$$17. \quad v = L \frac{di}{dt}$$

$$(a) \quad L \frac{di}{dt} = (5 \times 10^{-6}) 30 \times 10^{-9} [e^{-t} - te^{-t}] = 150(1-t)e^{-t} \text{ fV}$$

(b)

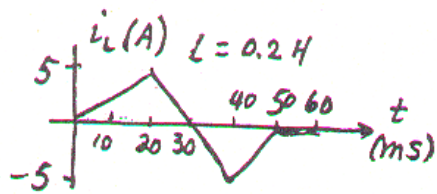
$$L \frac{di}{dt} = (5 \times 10^{-6})(4 \times 10^{-3}) [-5e^{-5t} \sin 100t + 100e^{-5t} \cos 100t]$$

$$\text{therefore } v = 100e^{-5t} (20 \cos 100t - \sin 100t) \text{ pV}$$

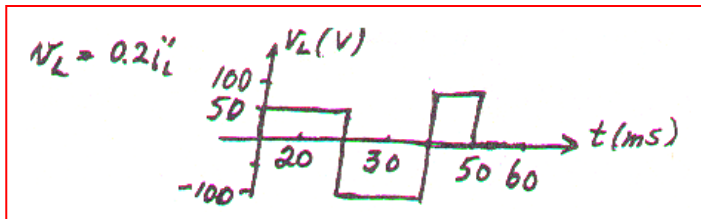
18.  $W = \frac{1}{2}LI^2$ . Maximum energy corresponds to maximum current flow, so

$$W_{\max} = \frac{1}{2}(5 \times 10^{-3})(1.5)^2 = 5.625 \text{ mJ}$$

19.



(a)



(b)  $P_L = v_L i_L \therefore P_{L\max} = (-100)(-5) = 500\text{W}$  at  $t = 40^- \text{ms}$

(c)  $P_{L\min} = 100(-5) = -500\text{W}$  at  $t = 20^+$  and  $40^+$  ms

(d)  $W_L = \frac{1}{2} L i_L^2 \therefore W_L(40\text{ms}) = \frac{1}{2} \times 0.2(-5)^2 = 2.5\text{J}$

20.

$$L = 50 \times 10^{-3}, t < 0: i = 0; t > 0 \quad i = 80te^{-100t} \text{ mA} = 0.08te^{-100t} \text{ A}$$

$$\therefore i' = 0.08e^{-100t} - 8te^{-100t} \quad \therefore 0.08 = 8t, t_m = 0.01\text{s}, |i|_{\max} = 0.08 \times 0.01e^{-1}$$

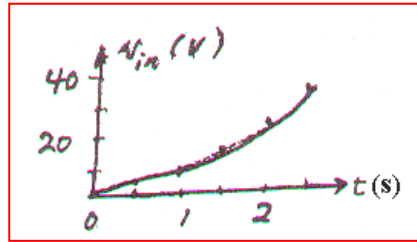
$$\therefore |i|_{\max} = 0.2943\text{mA}; v = 0.05i' = e^{-100t}(0.004 - 0.4t)$$

$$\therefore v' = e^{-100t}(-0.4) - 100e^{-100t}(0.004 - 0.4t) \quad \therefore -0.4 = 0.4 - 40t, t = \frac{0.8}{40} = 0.02\text{s}$$

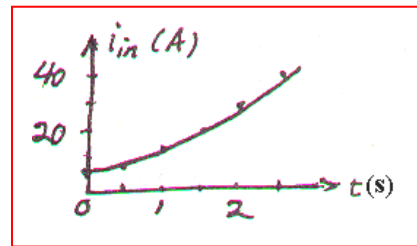
$$v = e^{-2}(0.004 - 0.008) = -0.5413\text{mV} \text{ this is minimum.} \therefore |v|_{\max} = 0.004\text{V at } t=0$$

21.

(a)  $t > 0: i_s = 0.4t^2 \text{ A} \therefore v_{in} = 10i_s + 5i_s' = 4t^2 + 4t \text{ V}$



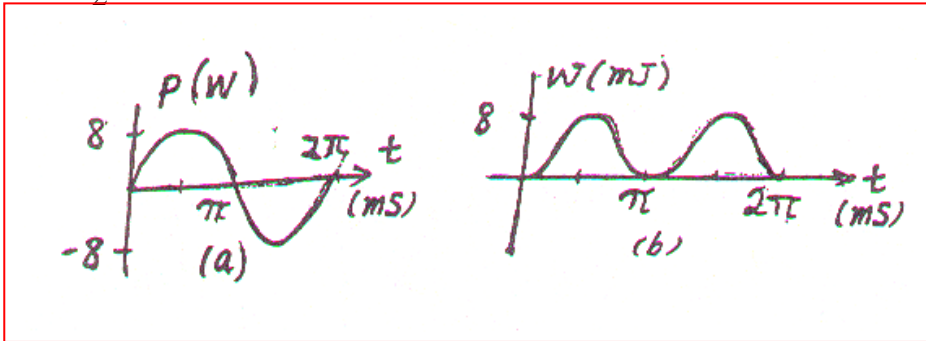
(b)  $i_{in'} = 0.1v_s + \frac{1}{5} \int_0^t 40t dt + 5 = 4t + 4t^2 + 5 \text{ A}$



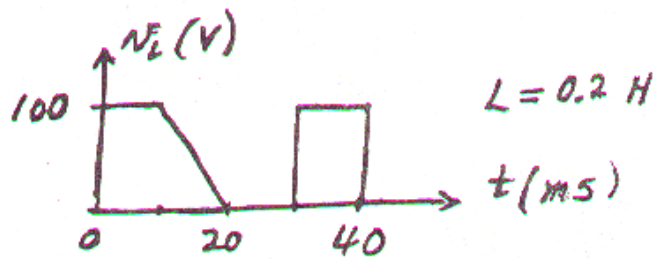
22.  $v_L = 20 \cos 1000t \text{ V}$ ,  $L = 25 \text{ mH}$ ,  $i_L(0) = 0$

(a)  $i_L = 40 \int_0^t 20 \cos 1000t dt = 0.8 \sin 1000t \text{ A}$ .  $\therefore p = 8 \sin 2000t \text{ W}$

(b)  $w = \frac{1}{2} \times 25 \times 10^{-3} \times 0.64 \sin^2 1000t = 8 \sin^2 1000t \text{ mJ}$



23.



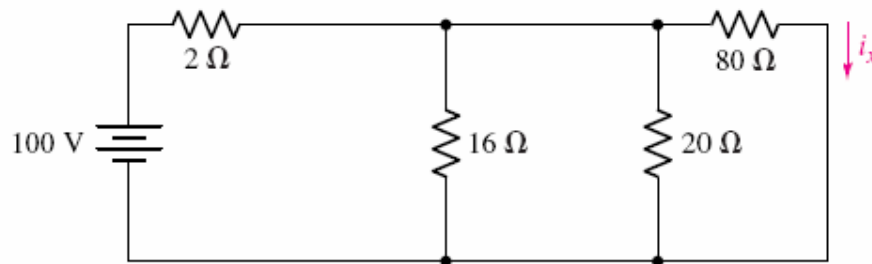
- (a)  $0 < t < 10 \text{ ms}$ :  $i_L = -2 + 5 \int_0^t 100 dt = -2 + 500t \therefore i_L(10\text{ms}) = 3\text{A}, i_L(8\text{ms}) = \boxed{2\text{A}}$
- (b)  $i_L(0) = 0 \therefore i_L(10\text{ms}) = 500 \times 0.01 = 5\text{A} \therefore i_L(20\text{ms}) = 5 + 5 \int_{0.01}^{0.02} 10^4(0.02 - t) dt$   
 $\therefore i_L(20\text{ms}) = 5 + 5 \times 10^4(0.02t - 0.5t^2)_{0.01}^{0.02} = 5 + 5 \times 10^4(0.0002 - 0.00015) = 7.5\text{A}$   
 $\therefore w_L = \frac{1}{2} \times 0.2 \times 7.5^2 = \boxed{5.625\text{J}}$
- (c) If the circuit has been connected for a long time, L appears like short circuit.

$$V_{8\Omega} = \frac{8}{2+8}(100\text{V}) = 80\text{V}$$

$$I_{2\Omega} = \frac{20\text{V}}{2\Omega} = 10\text{A}$$

$$\therefore i_x = \frac{80\text{V}}{80\Omega} = 1\text{A}$$

24. After a very long time connected only to DC sources, the inductors act as short circuits. The circuit may thus be redrawn as



$$\text{And we find that } i_x = \left( \frac{\frac{80}{9}}{80 + \frac{80}{9}} \right) \left( \frac{100}{2+8} \right) = \boxed{1 \text{ A}}$$



25.  $L = 5\text{H}, V_L = 10(e^{-t} - e^{-2t})\text{V}, i_L(0) = 0.08\text{A}$

(a)  $v_L(1) = 10(e^{-1} - e^{-2}) = 2.325\text{ V}$

(b)  $i_L = 0.08 + 0.2 \int_0^t 10(e^{-t} - e^{-2t}) dt = 0.08 + 2(-e^{-t} + 0.5e^{-2t})_0^t$

$$i_L = 0.08 + 2(-e^{-t} + 0.5e^{-2t} + 1 - 0.5) = 1.08 + e^{-2t} - 2e^{-t} \therefore i_L(1) = 0.4796\text{A}$$

(c)  $i_L(\infty) = 1.08\text{A}$

26.

$$\begin{aligned} \text{(a)} \quad v_x &= 120 \times \frac{40}{12 + 20 + 40} + 40 \times 5 \times \frac{12}{12 + 20 + 40} \\ &= \frac{200}{3} + \frac{100}{3} = \boxed{100\text{V}} \end{aligned}$$

$$\begin{aligned} \text{(b)} \quad v_x &= \frac{120}{12 + 15 \parallel 60} \times \frac{15}{15 + 60} \times 40 + 40 \times 5 \frac{15 \parallel 12}{15 \parallel 12 + 60} \\ &= \frac{120}{12 + 12} \times \frac{1}{5} \times 40 + 200 \frac{6.667}{66.667} \\ &= 40 + 20 = \boxed{60\text{V}} \end{aligned}$$

27.

(a)  $w_L = \frac{1}{2} \times 5 \times 1.6^2 = 6.4\text{J}$

(b)  $w_c = \frac{1}{2} \times 20 \times 10^{-6} \times 100^2 = 0.1\text{J}$

(c) Left to right (magnitudes): 100, 0, 100, 116, 16, 16, 0 (V)

(d) Left to right (magnitudes): 0, 0, 2, 2, 0.4, 1.6, 0 (A)

28.

$$(a) \quad v_s = 400t^2 \text{ V}, t > 0; i_L(0) = 0.5 \text{ A}; t = 0.4 \text{ s}$$

$$v_c = 400 \times 0.16 = 64 \text{ V}, w_c = \frac{1}{2} \times 10^{-5} \times 64^2 = \boxed{20.48 \text{ mJ}}$$

$$(b) \quad i_L = 0.5 + 0.1 \int_0^{0.4} 400t^2 dt = 0.5 + 40 \times \frac{1}{3} \times 0.4^3 = 1.3533 \text{ A}$$

$$\therefore w_L = \frac{1}{2} \times 10 \times 1.3533^2 = \boxed{9.1581 \text{ J}}$$

$$(c) \quad i_R = 4t^2, P_R = 100 \times 16t^4 \therefore w_R = \int_0^{0.4} 1600t^4 dt = 320 \times 0.4^5 = \boxed{3.277 \text{ J}}$$

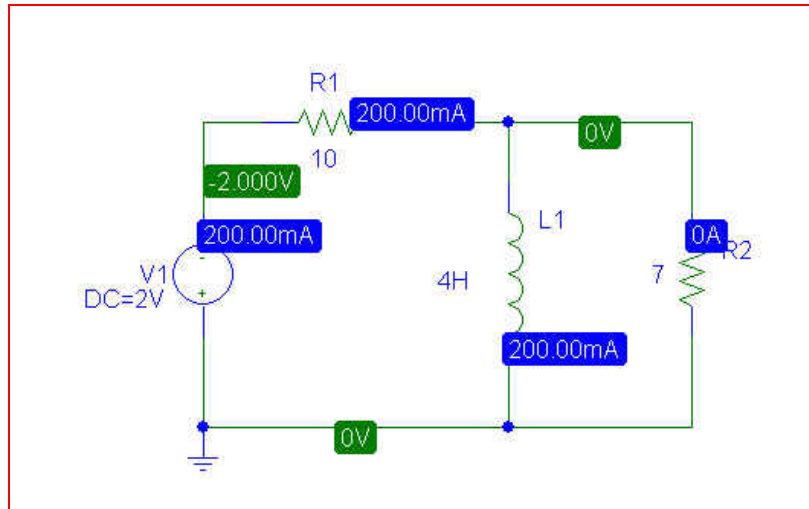
29. (a)  $P_{7\Omega} = 0W$ ;  $P_{10\Omega} = \frac{V^2}{R} = \frac{(2)^2}{10} = 0.4W$

(b) PSpice verification

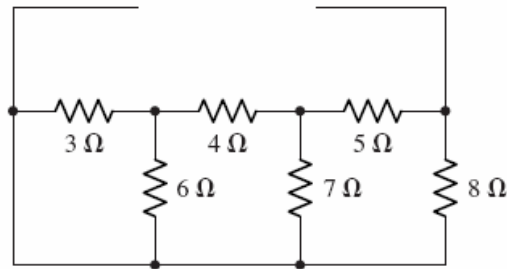
We see from the PSpice simulation that the voltage across the 10- $\Omega$  resistor is  $-2$  V, so that it is dissipating  $4/10 = 400$  mW.

The 7- $\Omega$  resistor has zero volts across its terminals, and hence dissipates zero power.

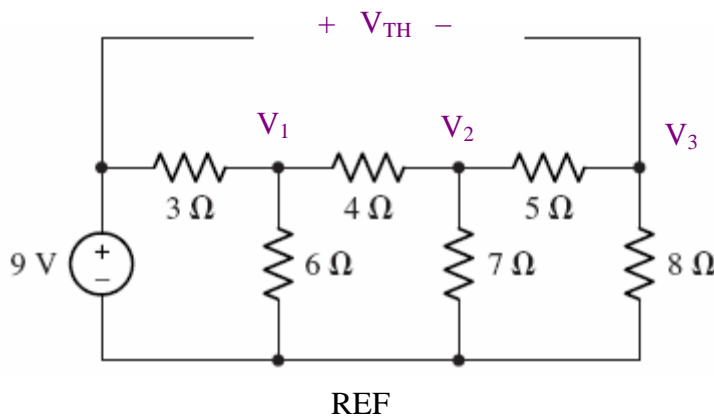
Both results agree with the hand calculations.



30. (a) We find  $R_{TH}$  by first short-circuiting the voltage source, removing the inductor, and looking into the open terminals.



Simplifying the network from the right,  $3 \parallel 6 + 4 = 6 \Omega$ , which is in parallel with  $7 \Omega$ .  
 $6 \parallel 7 + 5 = 8.23 \Omega$ . Thus,  $R_{TH} = 8.23 \parallel 8 = 4.06 \Omega$ . To find  $V_{TH}$ , we remove the inductor:

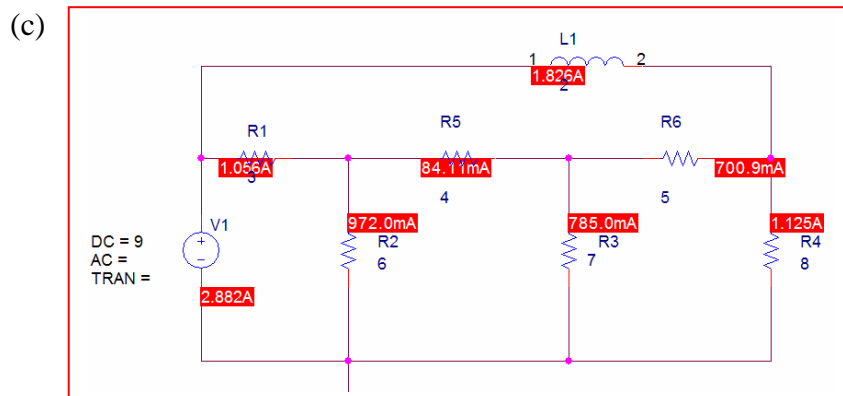


Writing the nodal equations required:

$$\begin{aligned} (V_1 - 9)/3 + V_1/6 + (V_1 - V_2)/4 &= 0 \\ (V_2 - V_1)/4 + V_2/7 + (V_2 - V_3)/5 &= 0 \\ V_3/8 + (V_3 - V_2)/5 &= 0 \end{aligned}$$

Solving,  $V_3 = 1.592 \text{ V}$ , therefore  $V_{TH} = 9 - V_3 = 7.408 \text{ V}$ .

(b)  $i_L = 7.408/4.06 = 1.825 \text{ A}$  (inductor acts like a short circuit to DC).



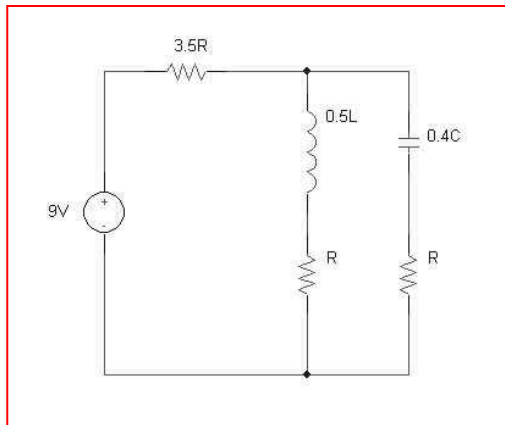
31.

$$C_{equiv} \equiv 10\mu + \left( \frac{1}{\frac{1}{10\mu} + \frac{1}{10\mu}} \right) \text{ in series with } 10\mu \text{ in series with } 10\mu + \left( \frac{1}{\frac{1}{10\mu} + \frac{1}{10\mu}} \right)$$
$$\equiv 4.286\mu F$$

$$32. \quad L_{equiv} \equiv (77 \mu\text{H} // (77 \mu\text{H} + 77 \mu\text{H})) + 77 \mu\text{H} + (77 \mu\text{H} // (77 \mu\text{H} + 77 \mu\text{H})) = 179.6 \mu\text{H}$$



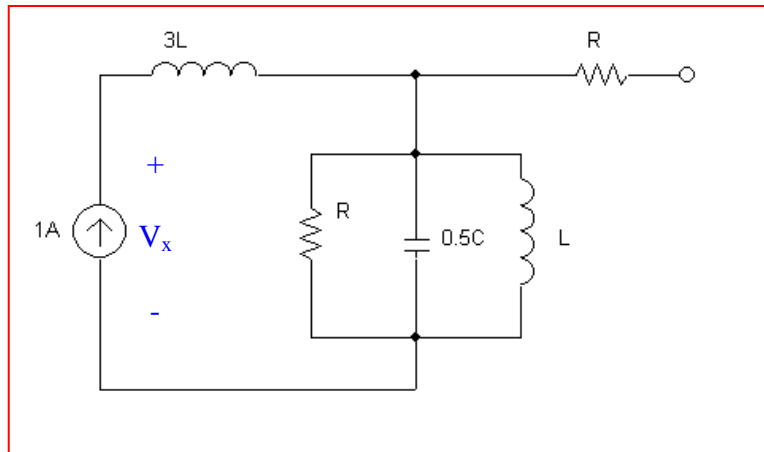
33. (a) Assuming all resistors have value  $R$ , all inductors have value  $L$ , and all capacitors have value  $C$ ,



- (b) At dc,  $20\mu\text{F}$  is open circuit;  $500\mu\text{H}$  is short circuit.

$$\text{Using voltage division, } V_x = \frac{10k}{10k + 15k}(9) = 3.6V$$

34. (a) As all resistors have value  $R$ , all inductors value  $L$ , and all capacitors value  $C$ ,



- (b)  $V_x = 0 \text{ V}$  as L is short circuit at dc.

35.  $C_{equiv} = \{ [(100 \text{ n} + 40 \text{ n}) \parallel 12 \text{ n}] + 75 \text{ n} \} \parallel \{ 7 \mu + (2 \mu \parallel 12 \mu) \}$

$$C_{equiv} \equiv 85.211 \text{ nF}$$

$$36. \quad L_{\text{equiv}} = \{[(17 \text{ p} \parallel 4 \text{ n}) + 77 \text{ p}] \parallel 12 \text{ n}\} + \{1 \text{ n} \parallel (72 \text{ p} + 14 \text{ p})\}$$

$$L_{\text{equiv}} \equiv 172.388 \text{ pH}$$

$$37. \quad C_T - C_x = (7 + 47 + 1 + 16 + 100) = 171 \mu F$$

$$E_{C_T - C_x} = \frac{1}{2} (C_T - C_x) V^2 = \frac{1}{2} (171 \mu)(2.5)^2 = 534.375 \mu J$$

$$E_{C_x} = E_{C_T} - E_{C_T - C_x} = (534.8 - 534.375) \mu J = 425 nJ$$

$$\therefore E_{C_x} = 425 n = \frac{1}{2} C_x V^2 \Rightarrow C_x = \frac{425 n(2)}{(2.5)^2} = 136 nF$$

38.

(a) For all  $L = 1.5H$ ,  $L_{equiv} = 1.5 + \left( \frac{1}{\frac{1}{1.5} + \frac{1}{1.5}} \right) + \left( \frac{1}{\frac{1}{1.5} + \frac{1}{1.5} + \frac{1}{1.5}} \right) = 2.75H$

(b) For a general network of this type, having  $N$  stages (and all  $L$  values equiv),

$$L_{equiv} = \sum_{N=1}^n \frac{L^N}{NL^{N-1}}$$

39.

$$(a) \quad L_{equiv} = 1 + \left( \frac{1}{\frac{1}{2} + \frac{1}{2}} \right) + \left( \frac{1}{\frac{1}{3} + \frac{1}{3} + \frac{1}{3}} \right) = 3H$$

(b) For a network of this type having 3 stages,

$$L_{equiv} = 1 + \frac{1}{\frac{2+2}{(2)^2}} + \frac{1}{\frac{3+3}{(3)^2} + \frac{1}{3}} = 1 + \frac{(2)^2}{2(2)} + \frac{(3)^3}{3(3)^2}$$

Extending for the general case of N stages,

$$\begin{aligned} L_{equiv} &= 1 + \frac{1}{\frac{1}{2} + \frac{1}{2}} + \frac{1}{\frac{1}{3} + \frac{1}{3} + \frac{1}{3}} + \dots + \frac{1}{\frac{1}{N} + \dots + \frac{1}{N}} \\ &= 1 + \frac{1}{2(1/2)} + \frac{1}{3(1/3)} + \dots + \frac{1}{N(1/N)} = N \end{aligned}$$

$$40. \quad C_{equiv} = \frac{(3p)(0.25p)}{3p + 0.25p} = 0.231pF$$



$$41. \quad L_{equiv} = \frac{(2.3n)(0.3n)}{2.6n} = 0.2916nH$$

42. (a) Use 2 x 1 $\mu$ H in series with 4 x 1 $\mu$ H in parallel.
- (b) Use 2 x 1 $\mu$ H in parallel, in series with 4 x 1 $\mu$ H in parallel.
- (c) Use 5 x 1 $\mu$ H in parallel, in series with 4 x 1 $\mu$ H in parallel.

43.

$$(a) \quad R = 10\Omega : 10\parallel 10\parallel 10 = \frac{10}{3}, \frac{10}{3} + 10 + 10\parallel 10 = \frac{55}{3}$$

$$\therefore R_{eq} = \frac{55}{3}\parallel 30 = 11.379\Omega$$

$$(b) \quad L = 10H \therefore L_{eq} = 11.379H$$

$$(c) \quad C = 10F : \frac{1}{1/30 + 1/10 + 1/20} = 5.4545$$

$$\therefore C_{eq} = 5.4545 + \frac{10}{3} = 8.788F$$

44.

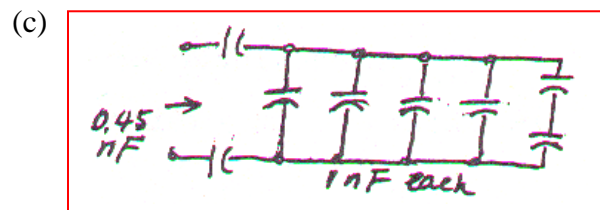
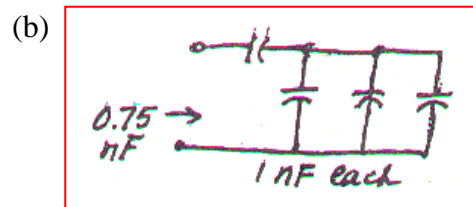
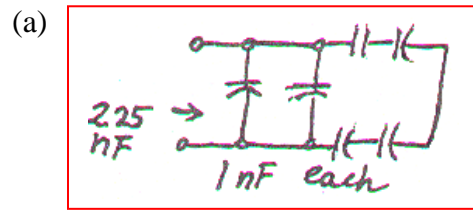
$$(a) \quad oc : L_{eq} = 6 \parallel 1 + 3 = 3.857H$$

$$sc : L_{eq} = (3 \parallel 2 + 1) \parallel 4 = 2.2 \parallel 4 = 1.4194H$$

$$(b) \quad oc : 1 + \frac{1}{1/4 + 1/2} = \frac{7}{3}, C_{eq} = \frac{1}{3/7 + 1/2} = 1.3125F$$

$$sc : \frac{1}{1/5 + 1} = \frac{5}{6}, C_{eq} = 4 + \frac{5}{6} = 4.833F$$

45.



46.  $i_s = 60e^{-200t}$  mA,  $i_1(0) = 20$  mA

(a)  $6 \parallel 4 = 2.4 \text{ H} \therefore v = L_{eq} i_s' = 2.4 \times 0.06(-200)e^{-200t}$   
or  $v = -28.8e^{-200t}$  V

(b)  $i_1 = \frac{1}{6} \int_0^t -28.8e^{-200t} dt + 0.02 = \frac{4.8}{200}(e^{-200t} - 1) + 0.02$   
 $= 24e^{-200t} - 4 \text{ mA}(t > 0)$

(c)  $i_2 = i_s - i_1 = 60e^{-200t} - 24e^{-200t} + 4 = 36e^{-200t} + 4 \text{ mA}(t > 0)$

$$47. \quad v_s = 100e^{-80t} \text{V}, v_1(0) = 20 \text{V}$$

$$(a) \quad i = C_{eq} v_s' = 0.8 \times 10^{-6} (-80) 100e^{-80t} = -6.4 \times 10^{-3} e^{-80t} \text{A}$$

$$(b) \quad v_1 = 10^6 (-6.4 \times 10^{-3}) \int_0^t e^{-80t} dt + 20 = \frac{6400}{80} (e^{-80t} - 1) + 20$$
$$\therefore v_1 = 80e^{-80t} - 60 \text{V}$$

$$(c) \quad v_2 \frac{10^6}{4} (-6.4 \times 10^{-3}) \int_0^t e^{-80t} dt + 80 = \frac{1600}{80} (e^{-80t} - 1) + 80$$
$$= 20e^{-80t} + 60 \text{V}$$

48.

(a)

$$\frac{v_c - v_s}{20} + 5 \times 10^{-6} v_c' + \frac{v_c - v_L}{10} = 0$$
$$\frac{v_L - v_c}{10} + \frac{1}{8 \times 10^{-3}} \int_0^t v_L dt + 2 = 0$$

(b)

$$20i_{20} + \frac{1}{5 \times 10^{-6}} \int_0^t (i_{20} - i_L) dt + 12 = v_s$$
$$\frac{1}{5 \times 10^{-6}} \int_0^t (i_L - i_{20}) dt - 12 + 10i_L + 8 \times 10^{-3} i_L' = 0$$



49.

$$v_c(t): 30\text{mA}: 0.03 \times 20 = 0.6\text{V}, v_c = 0.6\text{V}$$

$$9\text{V}: v_c = 9\text{V}, 20\text{mA}: v_c = -0.02 \times 20 = 0.4\text{V}$$

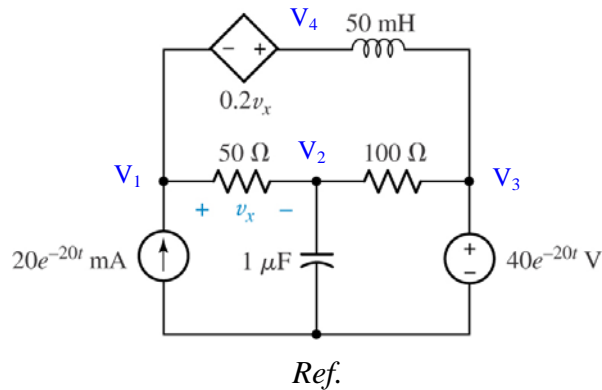
$$0.04 \cos 10^3 t: v_c = 0$$

$$\therefore v_c(t) = 9.2\text{V}$$

$$v_L(t): 30\text{mA}, 20\text{mA},$$

$$9\text{V}: v_L = 0; 0.04 \cos 10^3 t: v_L = -0.06 \times 0.04(-1000) \sin 10^3 t = 2.4 \sin 10^3 t \text{V}$$

50. We begin by selecting the bottom node as the reference and assigning four nodal voltages:



1, 4 Supernode:

$$20 \times 10^{-3} e^{-20t} = \frac{V_1 - V_2}{50} + 0.02 \times 10^3 \int_0^t (V_4 - 40e^{-20t'}) dt' \quad [1]$$

and:

$$V_1 - V_4 = 0.2 V_x \quad \text{or} \quad 0.8V_1 + 0.2 V_2 - V_4 = 0 \quad [2]$$

Node 2:

$$0 = \frac{V_2 - V_1}{50} + \frac{V_2 - 40e^{-20t}}{100} + 10^{-6} \frac{dV_2}{dt} \quad [3]$$

51. (a)  $R_i = \infty, R_o = 0, A = \infty \therefore v_i = 0 \therefore i = Cv_s'$   
 also  $0 + Ri + v_o = 0 \therefore v_o = -RCv_s'$   
 $-v_i + Ri - Av_i = 0, v_s = \frac{1}{c} \int idt + v_i$

(b)  $v_o = -Av_i \therefore v_i = \frac{-1}{A} v_o \therefore i = \frac{1+A}{R} v_i$   
 $\therefore v_s = \frac{1}{c} \int idt - \frac{1}{A} v_o = -\frac{1}{A} v_o + \frac{1+A}{RC} \int -\frac{v_o}{A} dt$   
 $\therefore Av_s' = -v_o' - \frac{1+A}{RC} v_o$  or  $v_o' + \frac{1+A}{RC} v_o + Av_s' = 0$

52. Place a current source in parallel with a 1-M $\Omega$  resistor on the positive input of a buffer with output voltage,  $v$ . This feeds into an integrator stage with input resistor,  $R_2$ , of 1-M $\Omega$  and feedback capacitor,  $C_f$ , of 1  $\mu$ F.

$$i = C_f \frac{dv_{c_f}}{dt} = 1.602 \times 10^{-19} \times \frac{\text{ions}}{\text{sec}}$$

$$0 = \frac{V_a - V}{1 \times 10^6} + C_f \frac{dv_{c_f}}{dt} = \frac{V_a - V}{1 \times 10^6} + 1.602 \times 10^{-19} \frac{\text{ions}}{\text{sec}}$$

$$0 = \frac{-V}{R_2} + C_f \frac{dv_{c_f}}{dt} = \frac{-V}{1 \times 10^6} + 1.602 \times 10^{-19} \frac{\text{ions}}{\text{sec}}$$

Integrating current with respect to  $t$ ,  $\frac{1}{R_2} \int_0^t v dt' = C_f (V_{c_f} - V_{c_f}(0))$

$$\frac{1.602 \times 10^{-19} \times \text{ions}}{R_2} = C_f V_{c_f}$$

$$V_{c_f} = V_a - V_{out} \Rightarrow V_{out} = \frac{-R_1}{R_2 C_f} \times 1.602 \times 10^{-19} \times \text{ions} \Rightarrow V_{out} = \frac{-1}{C_f} \times 1.602 \times 10^{-19} \times \text{ions}$$

$$R_1 = 1 \text{ M}\Omega, C_f = 1 \mu\text{F}$$

53.  $R = 0.5\text{M}\Omega$ ,  $C = 2\mu\text{F}$ ,  $R_i = \infty$ ,  $R_o = 0$ ,  $v_o = \cos 10t - 1\text{V}$

(a) Eq. (16) is:  $\left(1 + \frac{1}{A}\right)v_o = -\frac{1}{RC} \int_0^t \left(v_s + \frac{v_o}{A}\right) dt - v_c(0)$

$$\therefore \left(1 + \frac{1}{A}\right)v_o' = -\frac{1}{RC} \left(v_s + \frac{v_o}{A}\right) \therefore \left(1 + \frac{1}{A}\right)(-10 \sin 10t) = -1 \left(v_s + \frac{1}{A} \cos 10t - \frac{1}{A}\right)$$

$$\therefore v_s = \left(1 + \frac{1}{A}\right)10 \sin 10t + \frac{1}{A} - \frac{1}{A} \cos 10t \quad \text{Let } A = 2000$$

$$\therefore v_s = 10.005 \sin 10t + 0.0005 - 0.0005 \cos 10t$$

(b) Let  $A = \infty \therefore v_s = 10 \sin 10t\text{V}$

54. Create a op-amp based differentiator using an ideal op amp with input capacitor  $C_1$  and feedback resistor  $R_f$  followed by inverter stage with unity gain.

$$V_{out} = + \frac{R}{R} R_f C_1 \frac{dvs}{dt} = 60 \times \frac{1mV}{rpm} / \text{min}$$

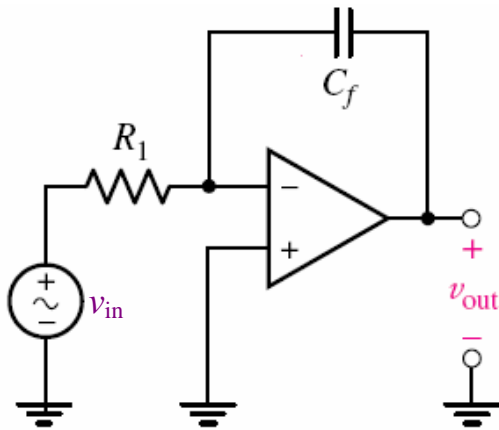
$R_f C_1 = 60$  so choose  $R_f = 6 \text{ M}\Omega$  and  $C_1 = 10 \mu\text{F}$ .

$$55. \quad (a) \quad 0 = \frac{1}{L} \int v dt + \frac{V_a - V_{out}}{R_f}$$

$$V_a = V = 0, \therefore \frac{1}{L} \int v_L dt = \frac{V_{out}}{R_f} \Rightarrow V_{out} = \frac{-R_f}{L} \int_0^t v_s dt'$$

(b) In practice, capacitors are usually used as capacitor values are more readily available than inductor values.

56. One possible solution:



$$v_{out} = -\frac{1}{R_1 C_f} \int v_{in} dt$$

we want  $v_{out} = 1$  V for  $v_{in} = 1$  mV over 1 s.

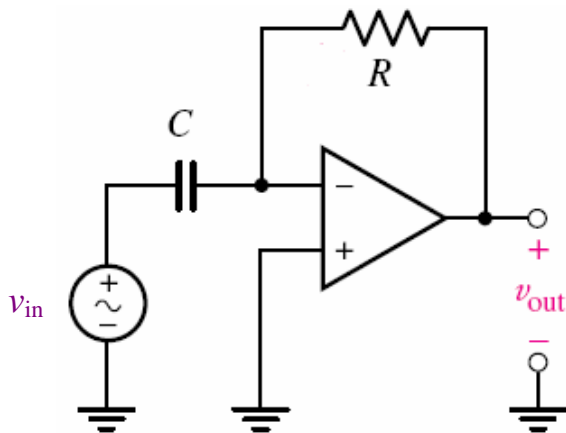
$$\text{In other words, } 1 = -\frac{1}{R_1 C_f} \int_0^1 10^{-3} dt = -\frac{10^{-3}}{R_1 C_f}$$

Neglecting the sign (we can reverse terminals of output connection if needed), we therefore need  $R_1 C_f = 10^{-3}$ .

Arbitrarily selecting  $C_f = 1 \mu\text{F}$ , we find  $R_1 = 1 \text{ k}\Omega$ .



57. One possible solution of many:



$$v_{out} = -RC \frac{dv_{in}}{dt}$$

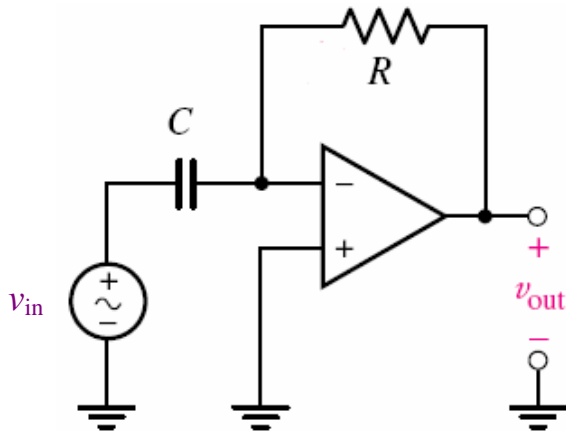
$$\text{maximum} \left( \frac{dv_{in}}{dt} \right) = \frac{100 \text{ mV}}{60 \text{ s}}$$

$$\text{In other words, } |v_{out}| = 1 \text{ V} = RC \left( \frac{100 \text{ mV}}{60 \text{ s}} \right)$$

$$\text{or } RC = 600$$

Arbitrarily selecting  $C = 1000 \mu\text{F}$ , we find that  $R = 600 \text{ k}\Omega$ .

58. One possible solution of many:



$$v_{out} = -RC \frac{dv_{in}}{dt}$$

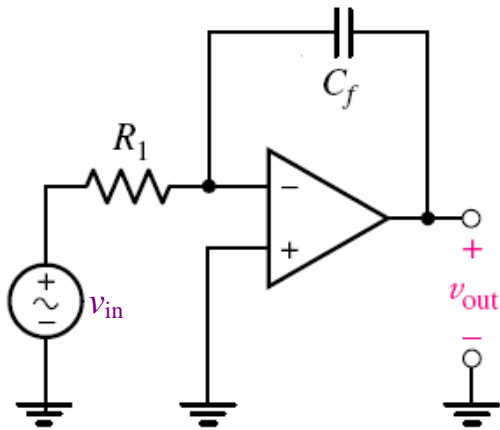
$$\text{At 1 litre/s, } \left( \frac{dv_{in}}{dt} \right) = \frac{100 \text{ mV}}{\text{s}}$$

$$\text{In other words, } |v_{out}| = 1 \text{ V} = RC \left( \frac{100 \text{ mV}}{1 \text{ s}} \right)$$

$$\text{or } RC = 10$$

Arbitrarily selecting  $C = 10 \mu\text{F}$ , we find that  $R = 1 \text{ M}\Omega$ .

59. One possible solution:



The power into a  $1\ \Omega$  load is  $I^2$ , therefore energy =  $W = I^2 \Delta t$ .

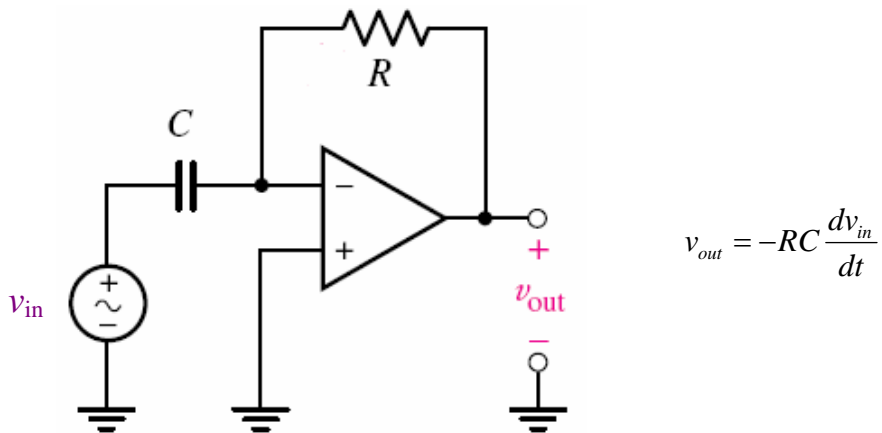
$$|v_{out}| = \frac{1}{R_1 C_f} \int I^2 dt$$

we want  $v_{out} = 1\ \text{mV}$  for  $v_{in} = 1\ \text{mV}$  (corresponding to  $1\ \text{A}^2$ ).

Thus,  $10^{-3} = RC(10^{-3})$ , so  $RC = 1$

Arbitrarily selecting  $C = 1\ \mu\text{F}$ , we find that we need  $R = 1\ \text{M}\Omega$ .

60. One possible solution of many:



Input: 1 mV = 1 mph, 1 mile = 1609 metres.

Thus, on the input side, we see 1 mV corresponding to 1609/3600 m/s.

Output: 1 mV per  $\text{m/s}^2$ . Therefore,

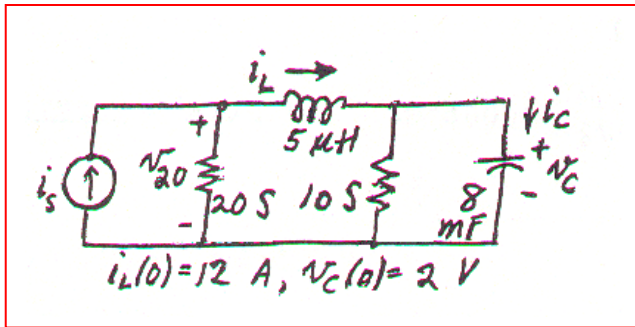
$$|v_{out}| = 2.237RC = 1$$

$$\text{so } RC = 0.447$$

Arbitrarily selecting  $C = 1 \mu\text{F}$ , we find that  $R = 447 \text{ k}\Omega$ .

61.

(a)



(b)

$$20v_{20} + \frac{1}{5 \times 10^{-6}} \int_0^t (v_{20} - v_c) dt + 12 = i_s$$

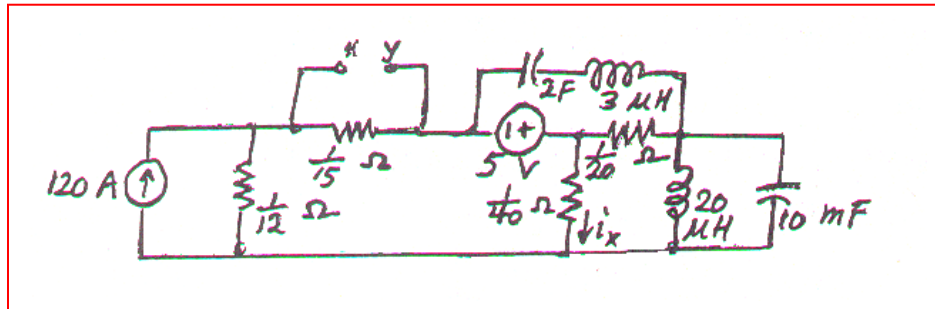
$$\frac{1}{5 \times 10^{-6}} \int_0^t (v_c - v_{20}) dt - 12 + 10v_c + 8 \times 10^{-3} v_c' = 0$$

(c)

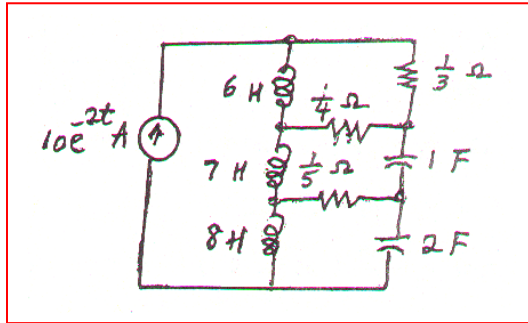
$$\frac{i_L - i_s}{20} + 5 \times 10^{-6} i_L' + \frac{i_L - i_c}{10} = 0$$

$$\frac{i_c - i_L}{10} + \frac{1}{8 \times 10^{-3}} \int_0^t i_c dt + 2 = 0$$

62.

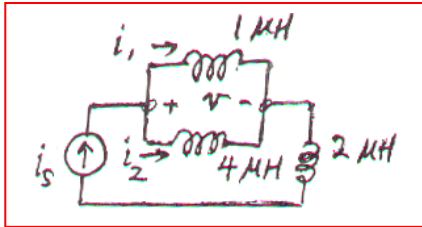


63.



64.

(a)

(b) “Let  $i_s = 100e^{-80t}$  A and  $i_1(0) = 20$  A in the circuit of (new) Fig. 7.62.(a) Determine  $v(t)$  for all  $t$ .(b) Find  $i_1(t)$  for  $t \geq 0$ .(c) Find  $v_2(t)$  for  $t \geq 0$ .”

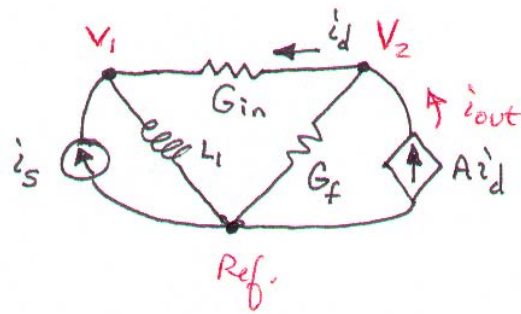
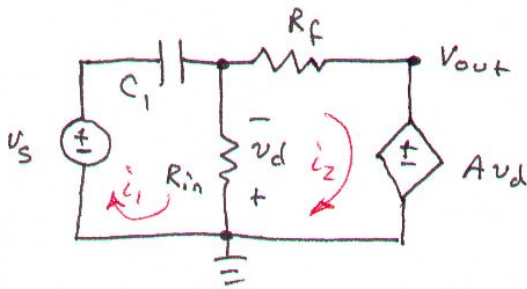
(c) (a)  $L_{eq} = 1 \parallel 4 = 0.8 \mu\text{H} \therefore v(t) = L_{eq} i_s' = 0.8 \times 10^{-6} \times 100(-80)e^{-80t} \text{ V}$   
 $\therefore v(t) = -6.43e^{-80t} \text{ mV}$

(b)  $i_1(t) = 10^6 \int_0^t -6.4 \times 10^{-3} e^{-80t} dt + 20 \therefore i_1(t) = \frac{6400}{80}(e^{-80t} - 1) = 80e^{-80t} - 60 \text{ A}$

(c)  $i_2(t) = i_s - i_1(t) \therefore i_2(t) = 20e^{-80t} + 60 \text{ A}$



65.



In creating the dual of the original circuit, we have lost both  $v_s$  and  $v_{out}$ . However, we may write the dual of the original transfer function:  $i_{out}/i_s$ . Performing nodal analysis,

$$i_s = \frac{1}{L_1} \int_0^t V_1 dt' + G_{in} (V_1 - V_2) \quad [1]$$

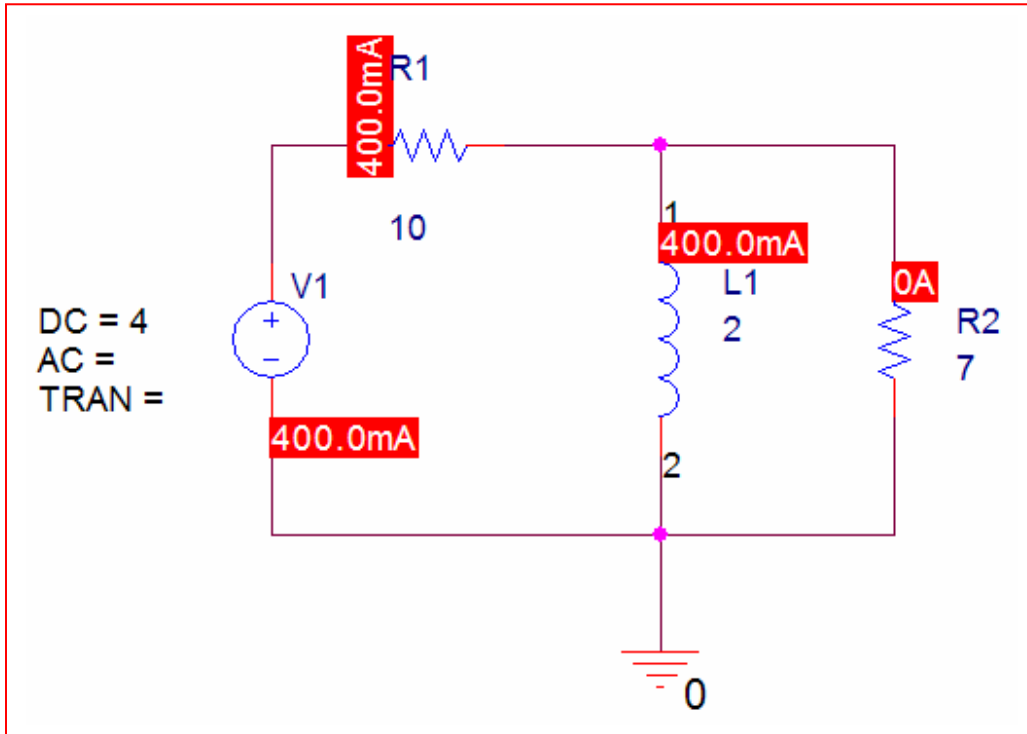
$$i_{out} = A i_d = G_f V_2 + G_{in} (V_2 - V_1) \quad [2]$$

Dividing, we find that

$$\frac{i_{out}}{i_s} = \frac{G_{in} (V_2 - V_1) + G_f V_2}{\frac{1}{L_1} \int_0^t V_1 dt' + G_{in} (V_1 - V_2)}$$

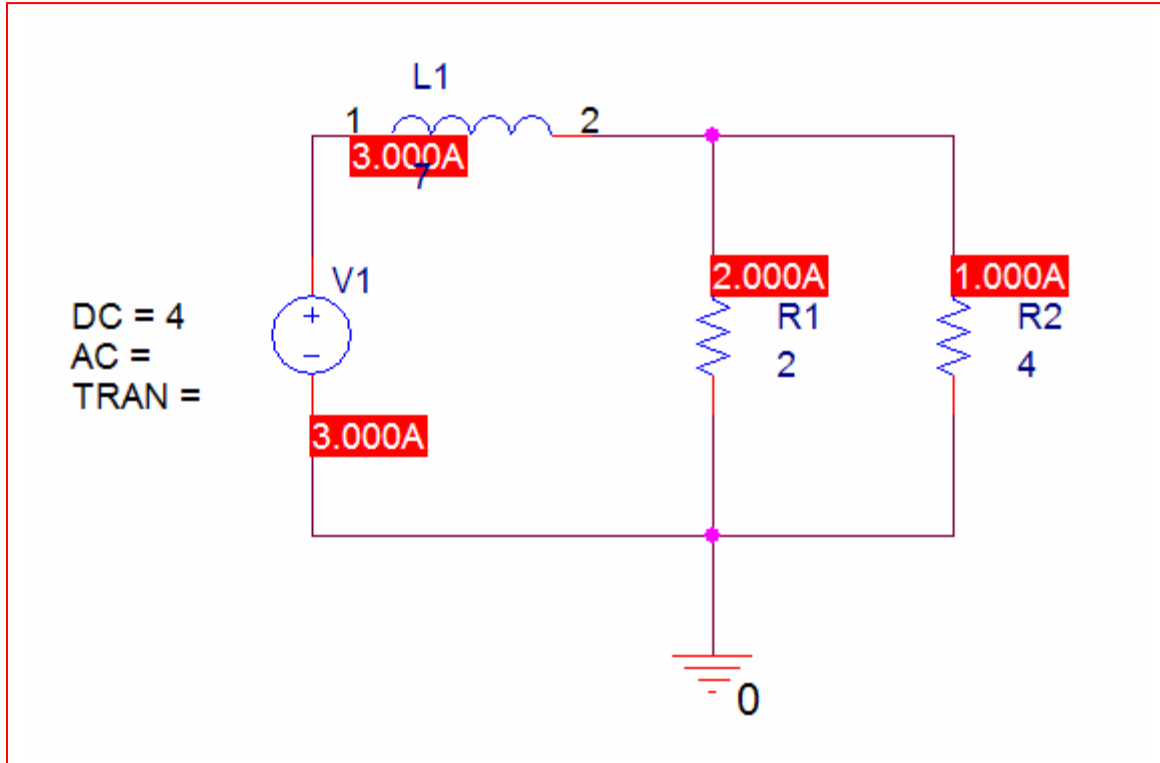
66.  $I_L = 4/10 = 400 \text{ mA}$ .  $W = \frac{1}{2}LI_L^2 = 160 \text{ mJ}$

PSpice verification:



67.  $I_L = 4/(4/3) = 3 \text{ A}$ .  $W = \frac{1}{2} LI_L^2 = 31.5 \text{ J}$

PSpice verification:



68. We choose the bottom node as the reference node, and label the nodal voltage at the top of the dependent source  $V_A$ .

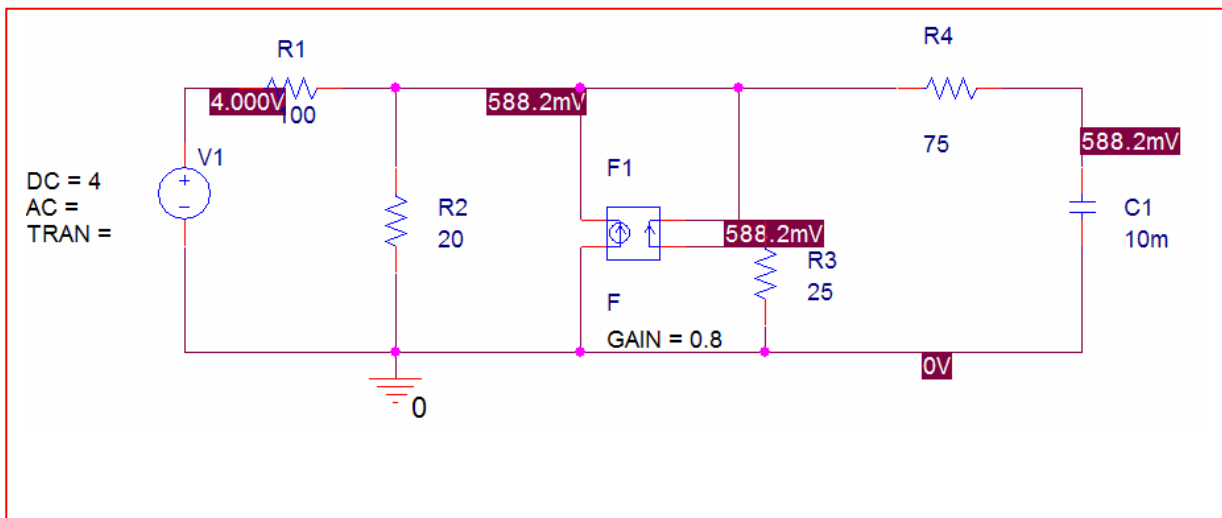
Then, by KCL,

$$\frac{V_A - 4}{100} + \frac{V_A}{20} + \frac{V_A}{25} = 0.8 \frac{V_A}{25}$$

Solving, we find that  $V_A = 588 \text{ mV}$ .

Therefore,  $V_C$ , the voltage on the capacitor, is  $588 \text{ mV}$  (no DC current can flow through the  $75 \Omega$  resistor due to the presence of the capacitor.)

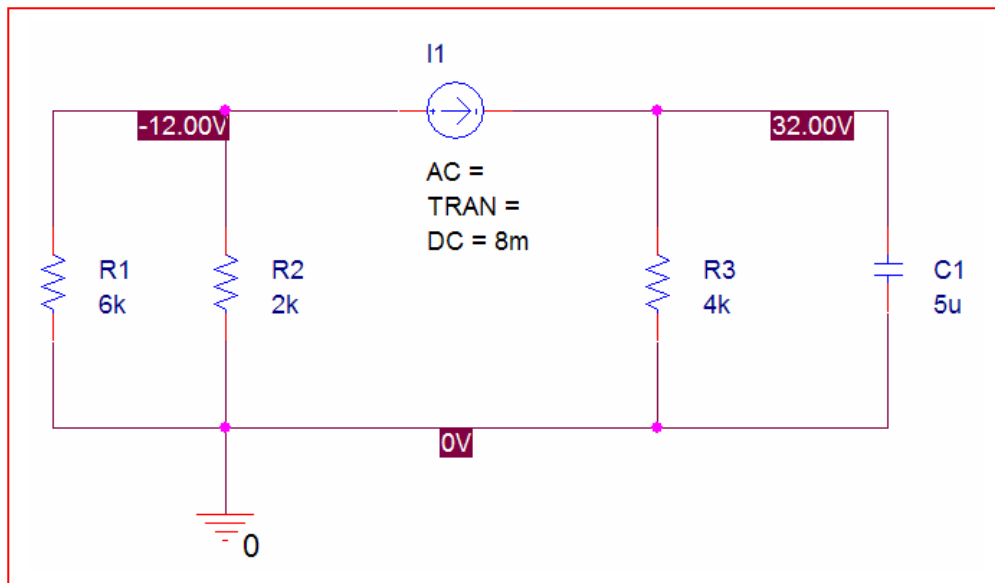
Hence, the energy stored in the capacitor is  $\frac{1}{2}CV^2 = \frac{1}{2}(10^{-3})(0.588)^2 = 173 \mu\text{J}$



69. By inspection, noting that the capacitor is acting as an open circuit, the current through the 4 k $\Omega$  resistor is 8 mA. Thus,  $V_c = (8)(4) = 32$  V.

$$\text{Hence, the energy stored in the capacitor} = \frac{1}{2}CV^2 = \frac{1}{2}(5 \times 10^{-6})(32)^2 = \boxed{2.56 \text{ mJ}}$$

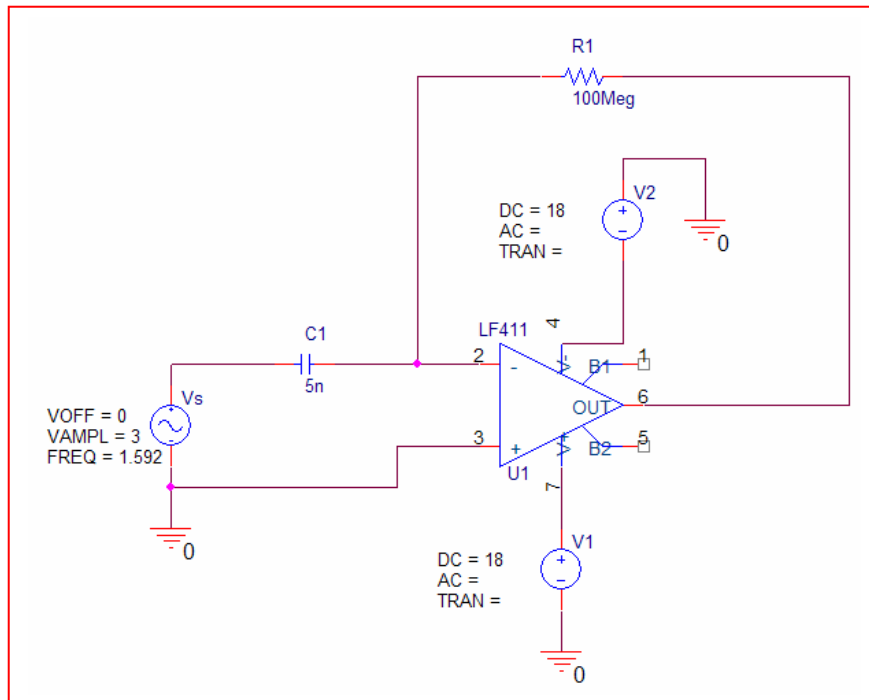
PSpice verification:



70.  $C_1 = 5 \text{ nF}$ ,  $R_f = 100 \text{ M}\Omega$ .

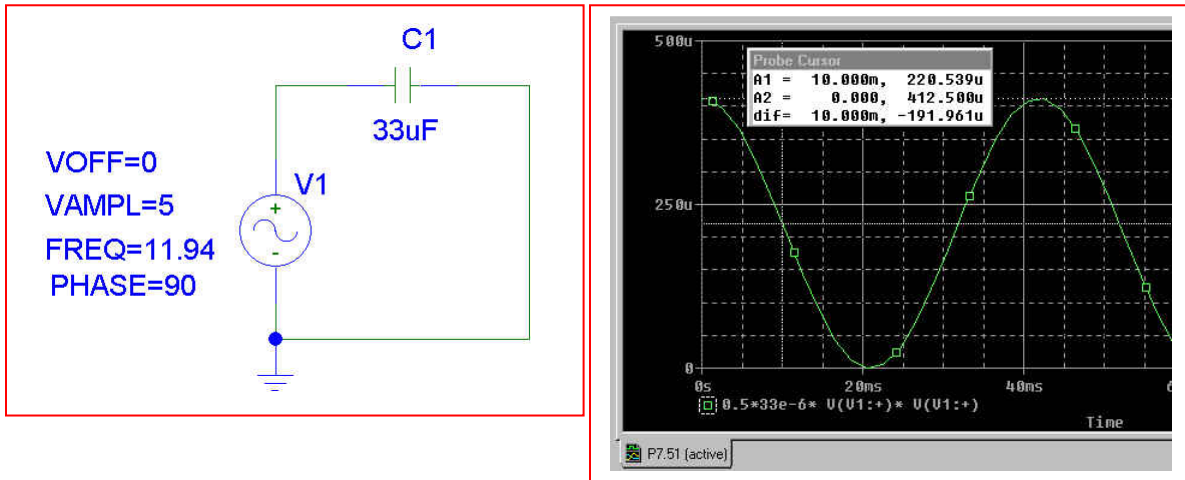
$$v_{out} = -R_f C_1 \frac{dv_s}{dt} = -(5 \times 10^{-9})(10^8)(30 \cos 100t) = -15 \cos 10t \text{ V}$$

Verifying with PSpice, choosing the LF411 and  $\pm 18 \text{ V}$  supplies:



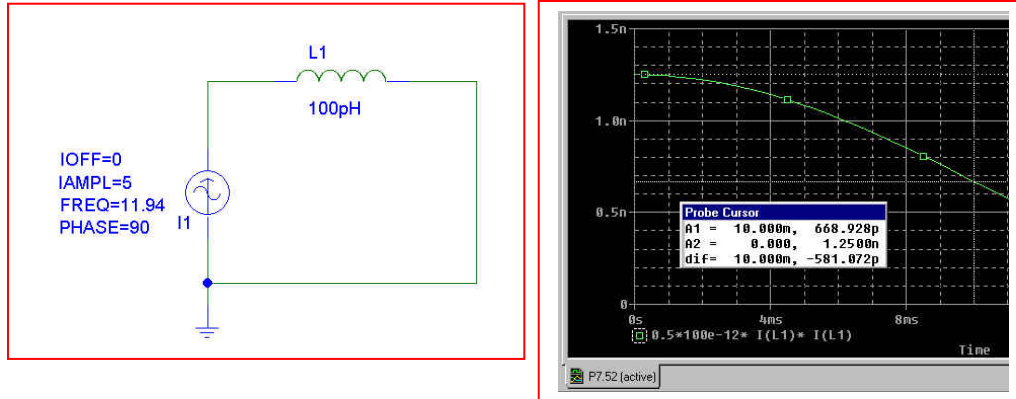
## 71. PSpice verification

$w = \frac{1}{2} C v^2 = 0.5 (33 \times 10^{-6}) [5 \cos (75 \times 10^{-2})]^2 = 220.8 \mu\text{J}$ . This is in agreement with the PSpice simulation results shown below.



## 72. PSpice verification

$w = \frac{1}{2} Li^2 = 0.5 (100 \times 10^{-12}) [5 \cos(75 \times 10^{-2})]^2 = 669.2 \text{ pJ}$ . This is in agreement with the PSpice simulation results shown below.





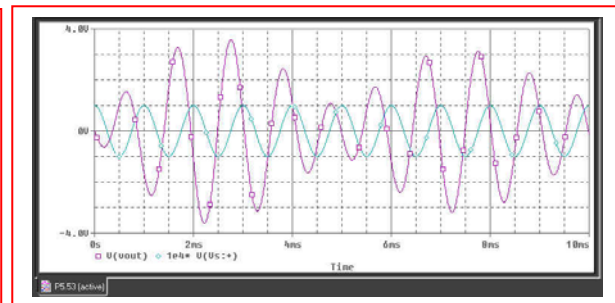
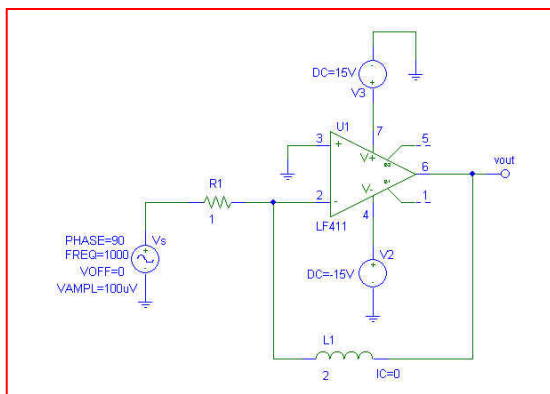
$$73. \quad 0 = \frac{V_a - V_s}{R_1} + \frac{1}{L} \int v_{L_f} dt$$

$$V_a = V_b = 0, \quad 0 = \frac{-V_s}{R_1} + \frac{1}{L} \int v_{L_f} dt$$

$$V_{L_f} = V_a - V_{out} = 0 - V_{out} = \frac{L}{R_1} \frac{dV_s}{dt}$$

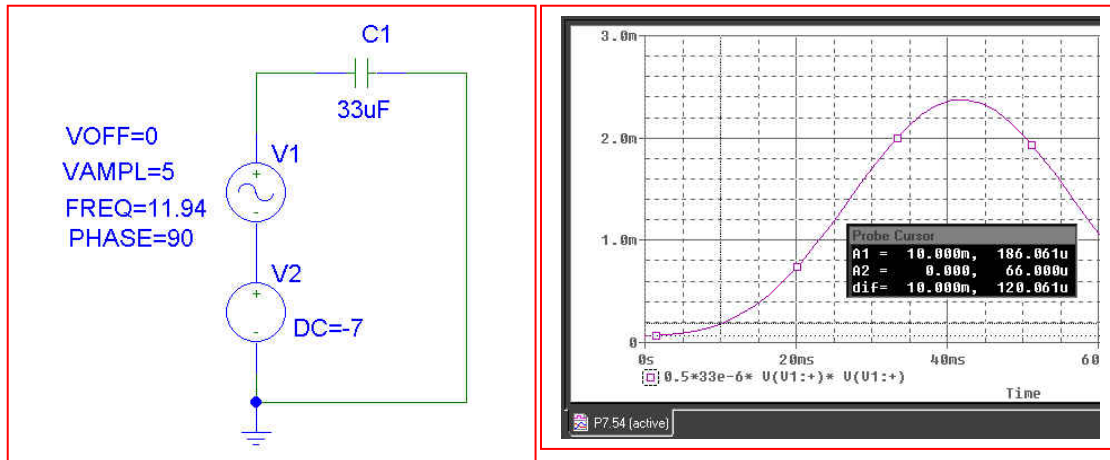
$$V_{out} = -\frac{L_f}{R_1} \frac{dV_s}{dt} = -\frac{L_f}{R_1} \frac{d}{dt} (A \cos 2\pi 10^3 t) \Rightarrow L_f = 2R_1; \text{ Let } R = 1 \Omega \text{ and } L = 1 \text{ H.}$$

PSpice Verification: clearly, something rather odd is occurring in the simulation of this particular circuit, since the output is not a pure sinusoid, but a combination of several sinusoids.



## 74. PSpice verification

$w = \frac{1}{2} C v^2 = 0.5 (33 \times 10^{-6}) [5 \cos (75 \times 10^{-2}) - 7]^2 = 184.2 \mu\text{J}$ . This is in reasonable agreement with the PSpice simulation results shown below.



## 75. PSpice verification

$w = \frac{1}{2} Li^2 = 0.5 (100 \times 10^{-12}) [5 \cos(75 \times 10^{-2}) - 7]^2 = 558.3 \text{ pJ}$ . This is in agreement with the PSpice simulation results shown below.

