



تقدم لجنة EiCoM الاكاديمية

تلخيص لمادة:

# مختبر تحكم آلي

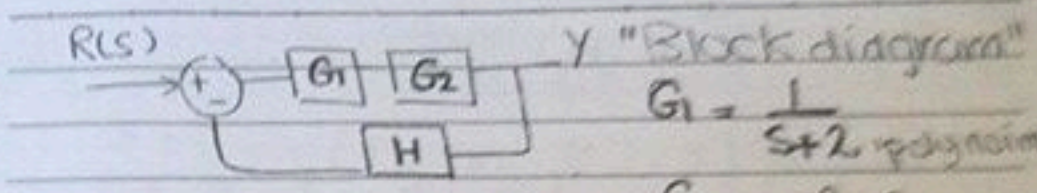




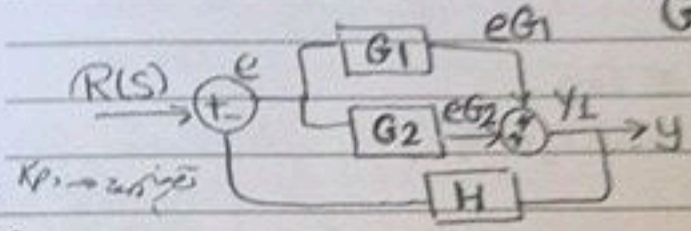
15/7/2014  
Tuesday

- Functions:-
- polyval
- conv
- roots
- series
- feedback
- parallel
- zero
- pole
- step
- minreal
- dc.gain
- clamp
- tf

No control lab.



"Block diagram"  
 $G_1 = \frac{1}{s+2}$  polynomial



$G_2 = \frac{1}{s^2+2}$   
 $2s^2-3s+1$

$p \rightarrow K_p \rightarrow$  error  
 $p \rightarrow K_p$   
 $I \rightarrow K_I \rightarrow$  poles

إذا كان  $G_1, G_2$  كالتالي  
error يتغير

"command window"  
Instruction

توصيف الـ  $s$  لا يعتمد على  
البيانات المتتالية  
Matrix

$a = [1]$

$b = [1 \ 2]$

$\text{polyval}(a, 0)$

$\text{polyval}(a, -10)$

بمنهج  $\text{command}$  الـ  $\text{matrix}$

$q = \text{polyval}(b, 0)$

$q = 2$

square prac.

$c = [1 \ 0 \ 2];$

$q = b * c$

$q = b \cdot c$

error  
b\*c size  
منه  
size

إذا كانت  $b$  و  $c$  متوافقين  
command  
يمكن  
work space

$q = \text{conv}(b, c)$

$q = [1 \ 2 \ 2 \ 4]$

$\text{roots}(q) \leftarrow$  round prac.

3 root

clear,clc  
تتميز النتائج  
بتميز قيم المتغيرات

$V = [1 \ 2 \ 3 \ 4 \ 5]$

$I = [1 \ 5 \ 7 \ 6 \ 3]$

$r = V / I$  error

$Y = V \cdot I$

$[ \dots ]$

نفس  
element

clear  
نفس كل شيء وكل شيء

per element

Polynomial  $\rightarrow$

Conv  $\rightarrow$

تحويل المتغيرات

يجب وضع  $\text{clc}$  عند بداية البرنامج



series → ZP, Poles  
parallel → ZP, Poles

No. \_\_\_\_\_

$G_1 = tF(a, b)$  transfer func.

$Y/R = \frac{G_1 G_2}{1 + F G_1 G_2 H}$

$G_2 = tF(c, [2 -3 4])$

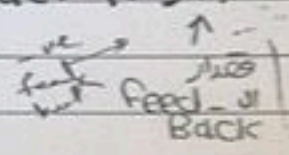
$\frac{F}{1 + FH}$

$Fw = G_1 * G_2$

$F = \text{series}(g_1, g_2)$  डिजिटल series transfer func.

$YR = \text{Feedback}(F, 1)$

-1 loop By default



$\frac{s^2 + 2}{2s^3 + 2s^2 - 2s + 10}$

unstable - 3 poles order

Zero (YR)  
pole (YR)

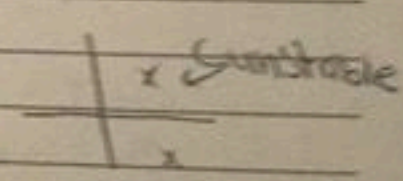
Feedback (for, Feed, +1) sign.

order 3

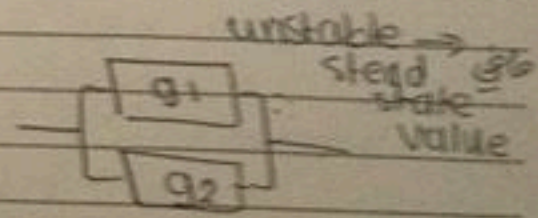
$s = -2.3403$   
 $0.6701 + 1.2991i$   
 $0.6701 - 1.2991i$   
unstable

unstable +ve feed back

real part right side



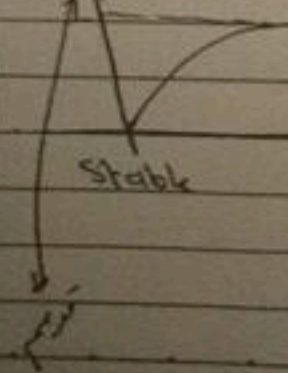
$F = g_1 + g_2$   
 $FF = \text{Parallel}(g_1, g_2)$



unstable → step state value

step response

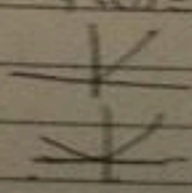
Step (ans)



behavioral first order

$d = \min \text{real}(a)$   
step d

$Y(0) = 0, Y(\infty) = 0$



step

Signature



No. 5

$\lim_{s \rightarrow 0} s Y(s) = \lim_{s \rightarrow 0} s T(s) R(s)$  to find steady state value.

$= \lim_{s \rightarrow 0} s \frac{1}{s+1} \frac{A}{s} = A$

initial input is unit step function

- $r = 5 * d$
- Step (a)  $\frac{1}{s}$
- Step (r)  $\frac{5}{s}$
- Step (5\*a)  $\frac{5}{s}$

initial condition is zero  
input is unit step function  
response is steady state

dc gain (d) ans = 1

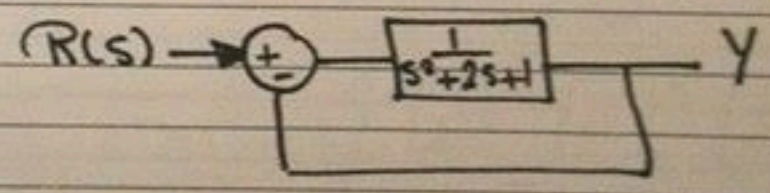
gain = 2, 1st order

dc gain (5\*d) ans = 5

2nd order system  
order  
damping ratio  
wn; natural freq.

damp(a) →

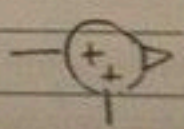
Simulink newmodule



minue

continuous → transfer fcn integrator

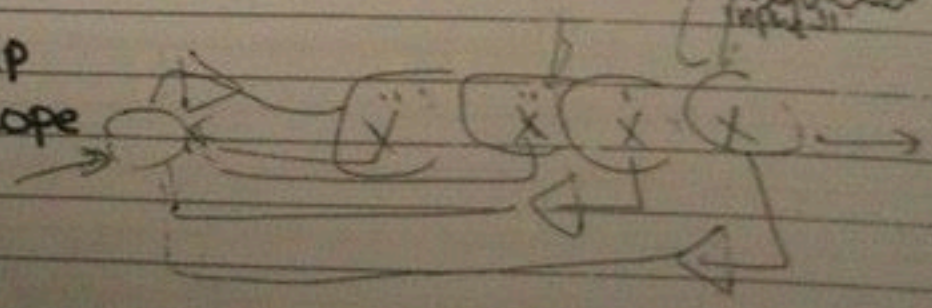
Math operation → sum gain



list of sign  
1 + -

Source → step

Sinks → scope



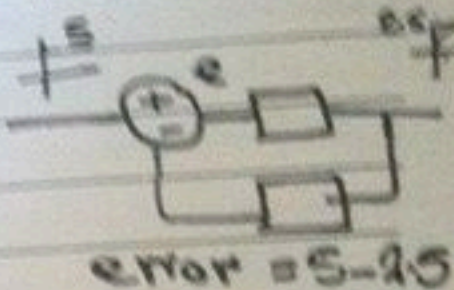


$$m\ddot{x} + b\dot{x} + cx = r(t)$$

$$mS^2 X(s) + bS X(s) + cX(s) = R(s)$$

$$m(S^2 X(s) + SX(0) + \dot{X}(0))$$

initial value  
initial condition



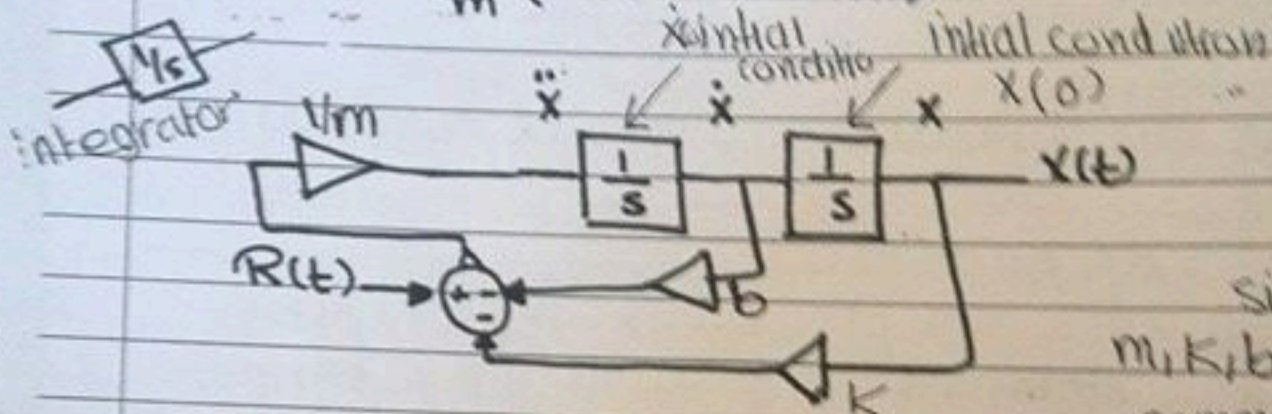
error = 5-25

$$m\ddot{x} + b\dot{x} + Kx = r(t)$$

$$\ddot{x} + \frac{b}{m}\dot{x} + \frac{K}{m}x = \frac{r(t)}{m}$$

$$\ddot{x} = \frac{1}{m}(r(t) - b\dot{x} - Kx)$$

1.  $\ddot{x}$  ditentukan  
2.  $\dot{x}$  ditentukan  
3.  $x$  ditentukan



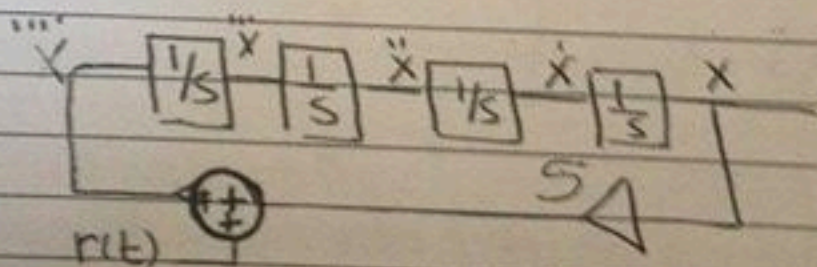
Block diagram

Simulink

command window

$$X - 5X = r(t)$$

$$\ddot{X} = 5X + r(t)$$





\* e = desired value - actual value

closed loop  $\frac{Y}{R} = \frac{G}{1+G}$

- ↑ G ↓ e (closed loop)  
- ↑ G ↑ e (open loop)

\* Sensitivity

$$S_G^T = \frac{\partial T}{\partial G} \times \frac{G}{T} = \frac{\Delta T}{\Delta G} \frac{G}{T}$$

G ↑ ↓ S

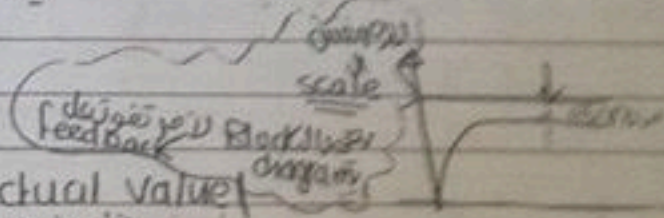
open loop, closed loop

unstable sys. if G is too large in closed loop

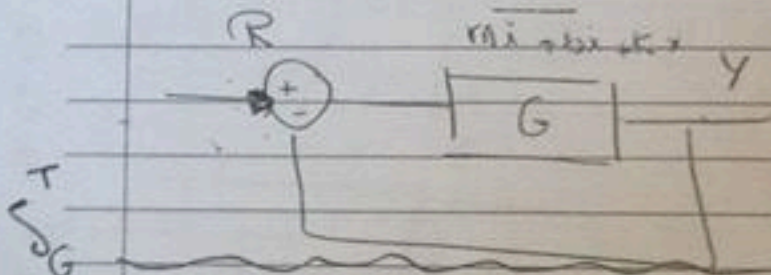
1) Accuracy (error analysis)

measurement of error

e = (desired value (Input) - actual value (Output))



e ↑ a ↓



closed loop  
 $\frac{Y}{R} = \frac{G}{1+G}$

2) Sensitivity

O.S.C.T

$S_G^T$  (Sensitivity of T w.r.t. G) is a parameter

closed loop  
open loop

$$S_G^T = \frac{\partial T}{\partial G} \times \frac{G}{T}$$

From above:

$$\frac{\Delta T}{\Delta G} \times \frac{G}{T}$$

0.5 0.3

$S_G^T$  ex.

$$\frac{Y}{R} = \frac{G G_1}{1 + G G_1}$$

$$\frac{\partial T}{\partial G} = \frac{G_1}{(1 + G G_1)^2}$$

↑ G, ↓ S

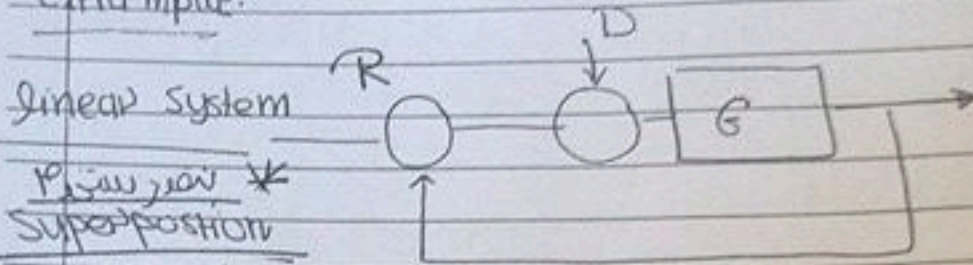


disturbance  
extra input

مداخل  
اضطراب

No.

disturbance Rejection (last condition) → Accuracy  
extra input.



Superposition

بسط  
الخطوات  
في  
الخطوات  
التي  
تليها  
الخطوات  
التي  
تليها

gain when D=0

$$Y = (D=0) R + (R=0) D$$

gain when R=0

استبدال

تحويل  
المعادلة

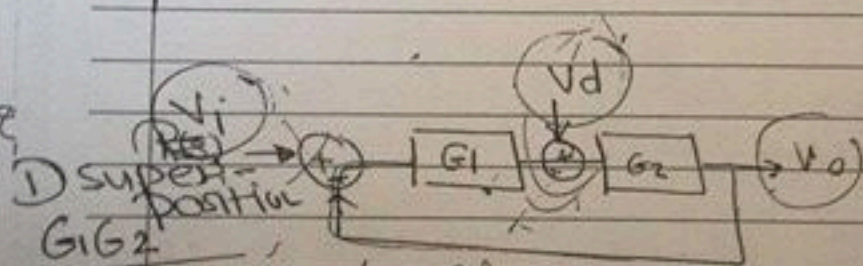
$$\frac{Y_D \times 100\%}{Y}$$

G	D
1	0
2	0
3	0
1	0

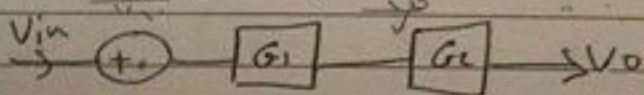
YR

$$Y_D \times 100\%$$

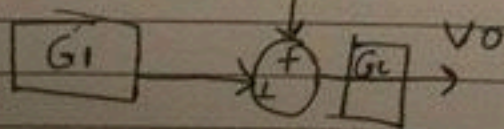
Y



$$V_{iH} (G_1 G_2) = \frac{V_o}{y_o}$$

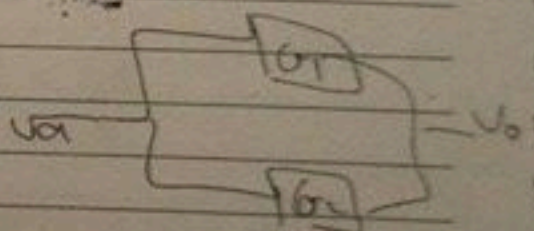
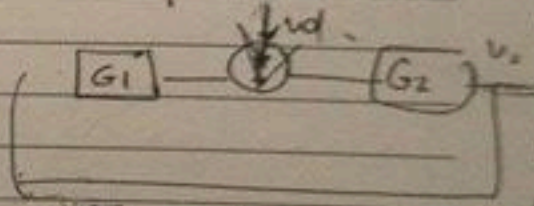


$$\frac{V_o}{V_{in}} = G_1 G_2 \checkmark$$



$$V_o = G_2$$

Vd





important

curves -  
parameters

no. control

2/2/2014

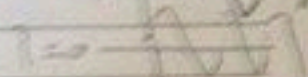
2nd order

$$T.F = \frac{K \omega^2}{s^2 + 2\zeta \omega_n s + \omega_n^2}$$

$K_p \neq 0$

$$* T.F = \frac{K \omega^2}{s^2 + 2\zeta \omega_n s + \omega_n^2}$$

$$s_{1,2} = -\zeta \omega_n \pm j \omega_n \sqrt{1 - \zeta^2}$$

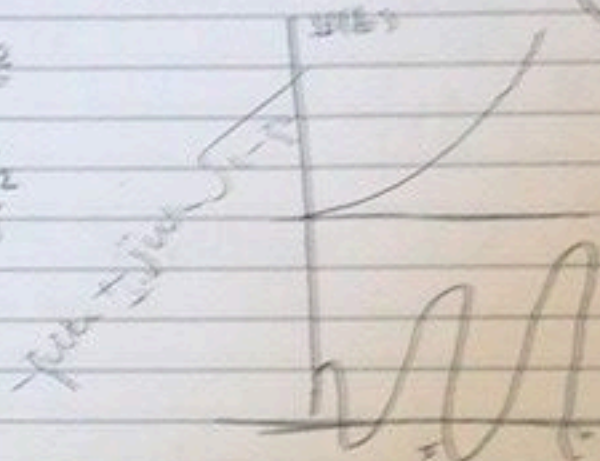


undamped

$$s_{1,2} = -\zeta \omega_n \pm j \omega_n \sqrt{1 - \zeta^2}$$

Overdamped Stable  
Real axis  
negative

$$-\zeta \omega_n \pm j \omega_n \sqrt{1 - \zeta^2}$$

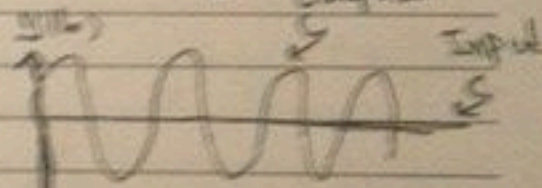
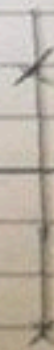


critical  
damped

undamped

$$\zeta = 0 \rightarrow s_{1,2} = \pm j \omega_n$$

critically stable



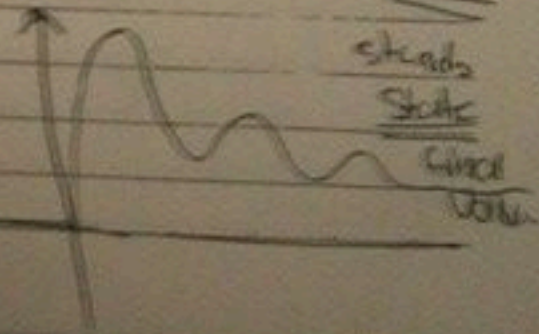
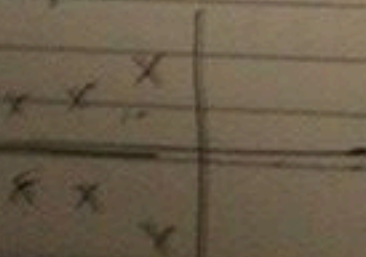
$$\omega = 2\pi f = \frac{2\pi}{T}$$

$\frac{K \omega_n^2}{\omega_n^2 + \zeta^2 \omega_n^2}$

$0 < \zeta < 1$  (under damped)

$$e^{-\zeta \omega_n t} + \omega_n$$

oscillation



steady state

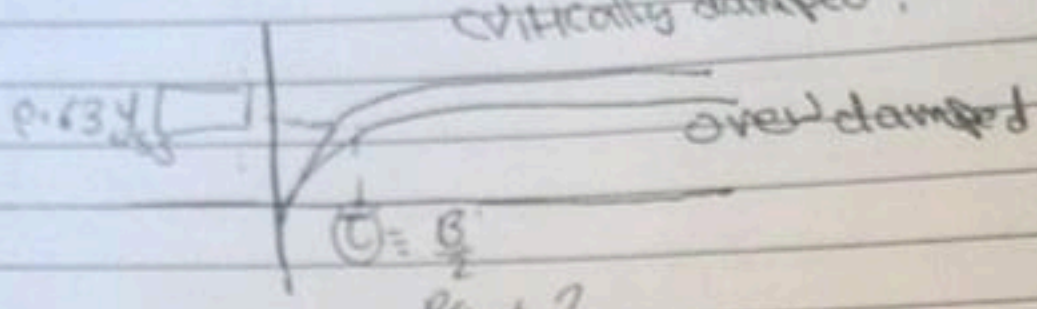
critical

(2/2)



$\zeta = 1 \rightarrow s_{1,2} = -\omega_n$

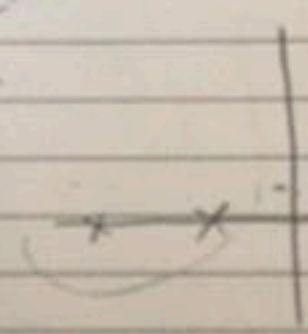
critically damped



second order system

$\tau_c = \frac{1}{R}$   
 $\frac{B\zeta + 2}{2}$   
 $\frac{B}{2} \zeta + 1$

$\zeta > 1$  two Real Roots.  $\rightarrow$  overdamped  
 damping Ratio.



$\frac{10^5}{2}$   
 $\frac{0.1}{10^5}$

$\tau_s = \frac{4}{\omega_n \zeta}$

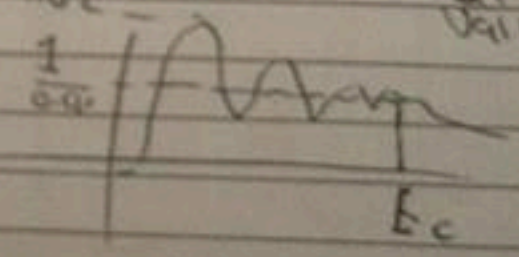
Approx

$\tau_p, \tau_r, \tau_s, \tau_d$   
 $\frac{4}{\omega_n \zeta}$

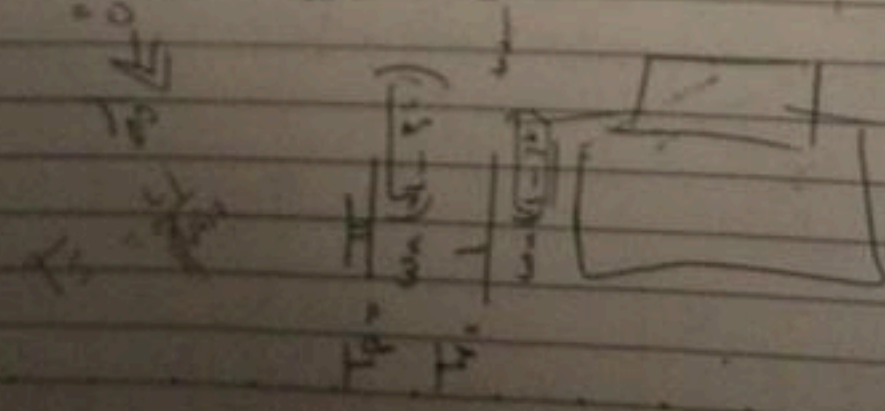
$1 - e^{-\zeta \omega_n t} \sin(\omega_d t)$

Final Value

Underdamped



Peak overshoot





$$\frac{Y(s)}{F(s)} = \frac{1}{ms^2 + bs + k}$$

not standard form

$$1 = s^2 \text{ (dobop, D)}$$

Calculus

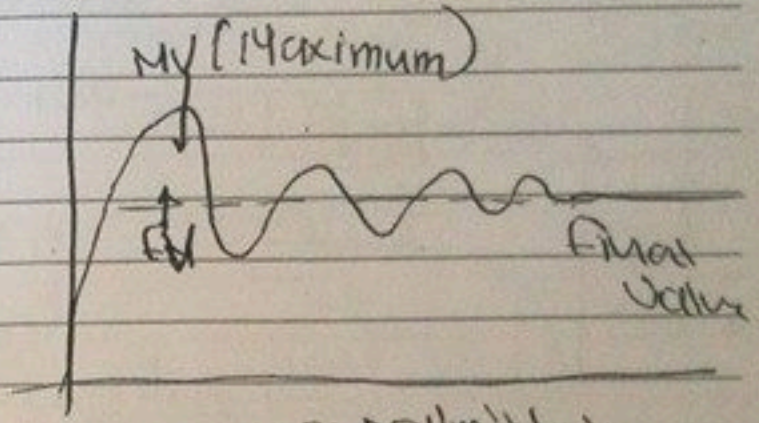
$$= \frac{1/m}{s^2 + \frac{b}{m}s + \frac{k}{m}}$$

RC

$$\omega_n = \sqrt{k/m}$$

$$k =$$

$$b =$$



theoretical

$$P_o = 100 e^{-\frac{3\pi}{\sqrt{1-\zeta^2}}} \%$$

exponential

$$P_o = \frac{MU - FU}{FU} \times 100\%$$

$$K = \frac{FV}{Input}$$

$$P_o = \frac{MU - FU}{FU} \times 100\%$$

$$P_o = \frac{MU - FU}{FU} \times 100\%$$

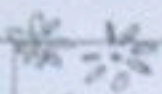
analysis

$$P_o = 100 e^{-\frac{3\pi}{\sqrt{1-\zeta^2}}} \%$$

$$P_o = \frac{MU - FU}{FU} \times 100\%$$

$$P_o = 100 e^{-\frac{3\pi}{\sqrt{1-\zeta^2}}}$$



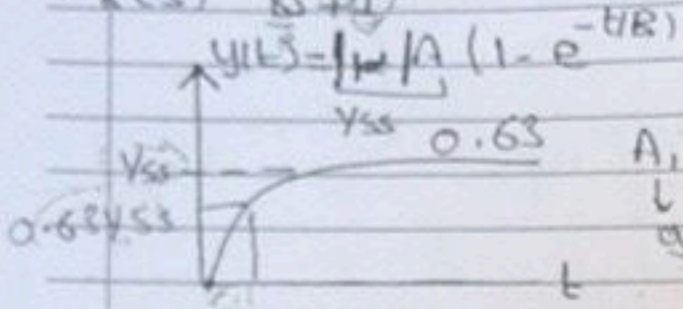


Control lab session 5  
5/8/2014

$$Y(s) = \frac{A}{Bs + 1}$$

Speed control of servo motor  
1st order system

$Y(s) = \frac{A}{Bs + 1}$  for the whole system  
Not for one block



A, B (parameters)

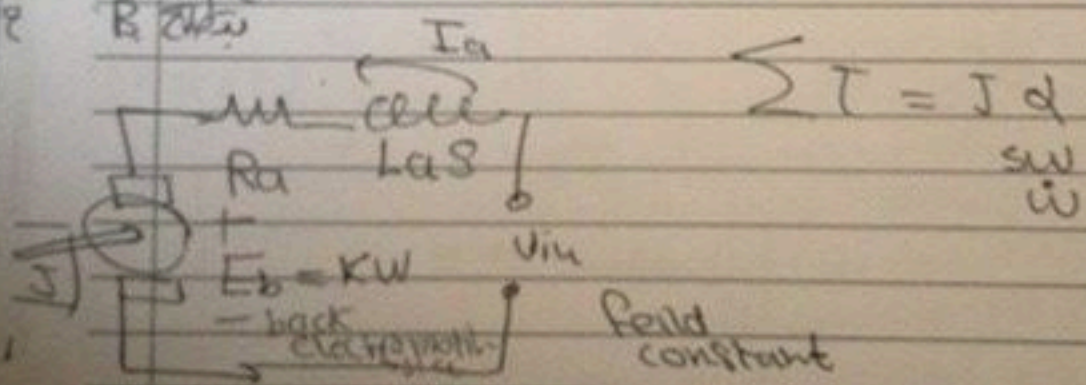
$$y(t) = |A|/|B| (1 - e^{-t/B})$$

$$y_{ss} = |A|/|B| =$$

$$A = \frac{y_{ss}}{|B|}$$

B → factor B (time constant)

قوت الی  
A 0.63  
B 0.63



$$T = K_2 I_a$$

$$\frac{W(s)}{V_{in}(s)} = \frac{K_m}{T_m s + 1}$$

When  $I_a = 0$

to reduce system order

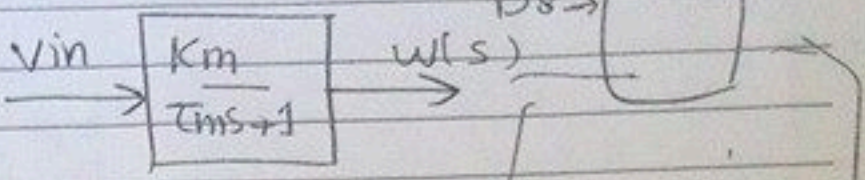
$I_a \neq 0 \rightarrow$  system is second order



$G_1 \rightarrow D_2$      $P_3 \rightarrow +S$   
 $G_2 \rightarrow B_2$      $F_6 \rightarrow f_1$      $A \times$   
 $D_3 \rightarrow B_3$      $D_5 \rightarrow D_4$   
 $F_1 \rightarrow f_6$      $F_8 \rightarrow P_8$   
 $D_8 \rightarrow$

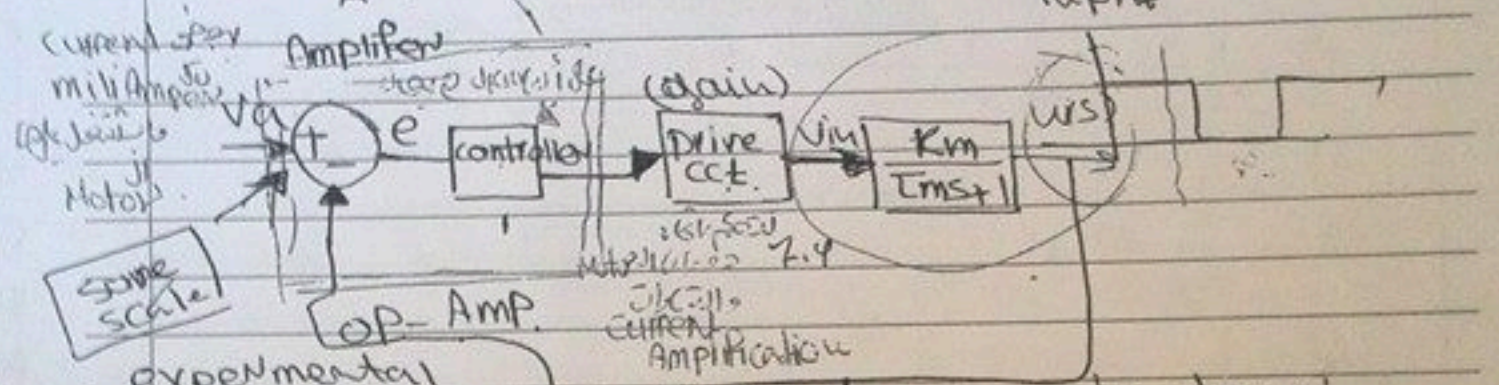
$B_1$   
 $B_2$   
 $B_3$

desired speed:-  
 (of motor, load)  
 (of controller)



$K_m$ ,  $T_m$   
 A                  B

Square wave  
 step input



experimental  
 one block.

tachogenerator  
 switch open/closed  
 2. Hz/v or  
 to draw curves!

servo Am  
 clockwise  
 servo motor  
 value 100V

to convert if closed loop system  
 we need to something convert.  
 mechanical to electrical (Small generator)  
 first order.

The resultant parameter of from the curves  
 are not  $K_m, T_m$ .

tachogenerator  
 - voltage given  
 - speed feedback  
 - speed indicator

$$\frac{A}{Ts+1}$$

$K_t$   
 $K_m$   
 $K_t$

gain of 1/s

~~1/s~~

$K_t$



## position control

$$v = \dot{x}$$

$$v = \dot{x}$$

$$\omega = \dot{\theta}$$

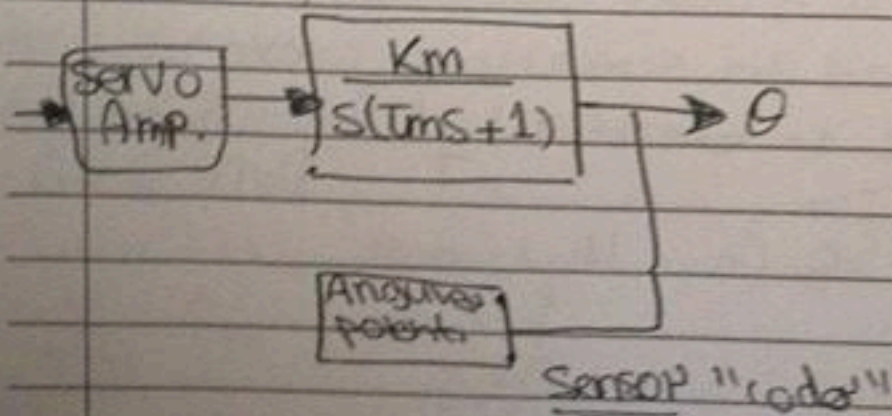
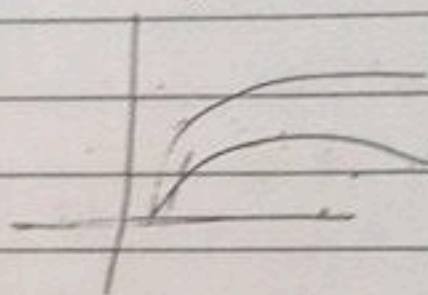
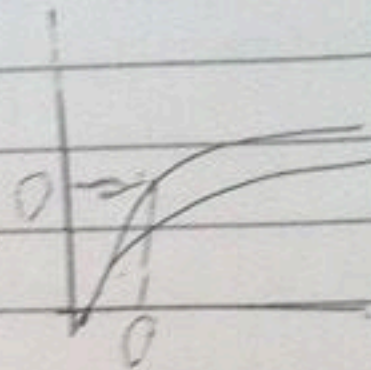
$$\theta = \int \omega = \frac{1}{s} \omega$$

$$\theta = \frac{1}{s} \omega = \frac{1}{s^2}$$

$$\theta = \frac{1}{s} \frac{K}{Tms+1} \quad (Ia=0)$$

$$\theta = \frac{1}{s^2} \frac{K}{Tms+1}$$

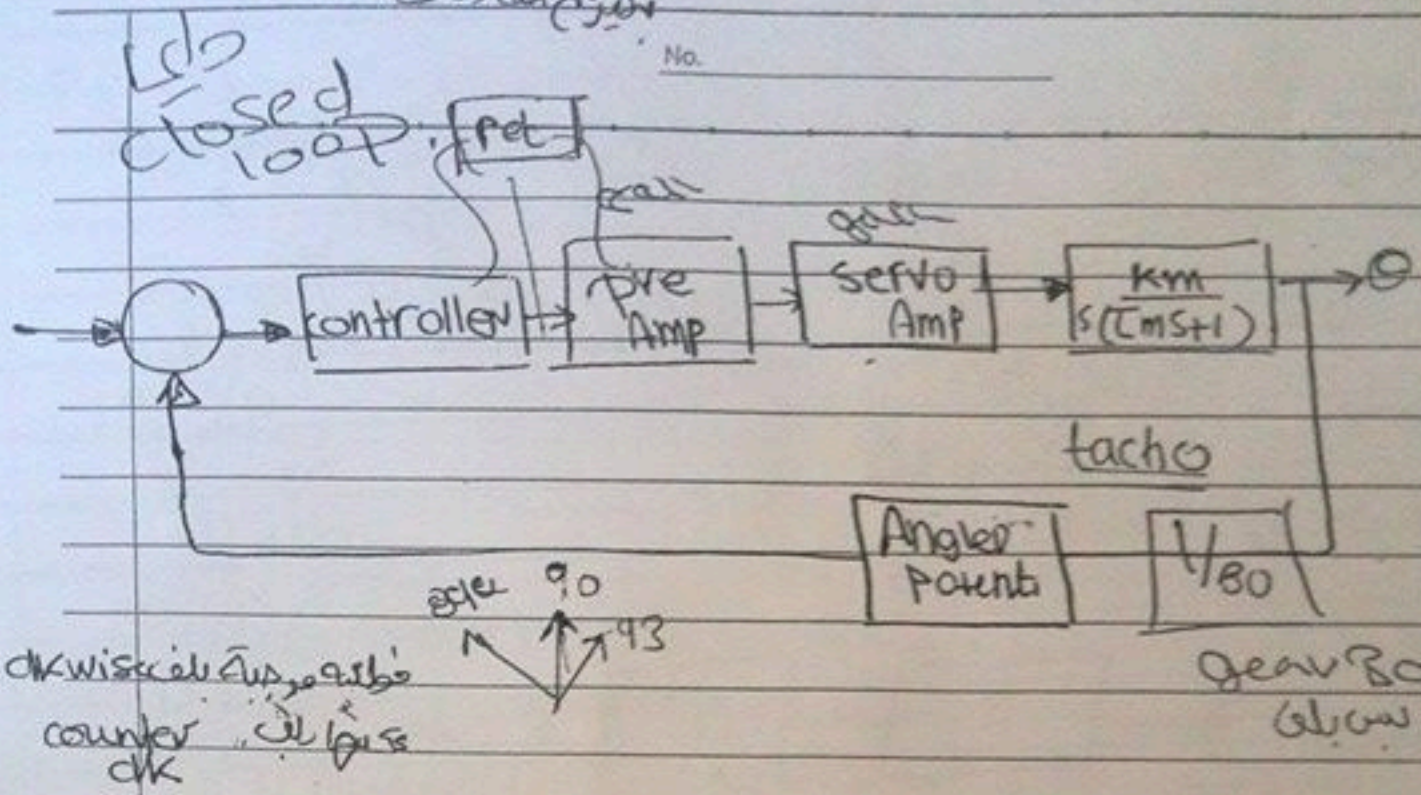
$$\theta = \int \omega = \frac{1}{s} \omega$$



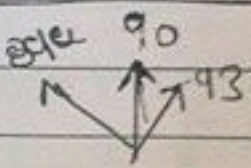


Control System

No. \_\_\_\_\_



دیسک سے تاحیہ  
counter  
دیسک



Gear Box  
1/80

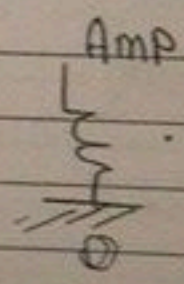
PreAMP signal from controller (+ve or negative)

+	H1 L2	CW
-	H2 L1	CCW

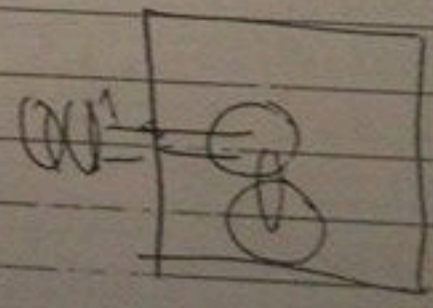


open loop  
unstable

2.50  
power amplifier  
speed control  
power 2.50  
reverses



Manual  
multistage

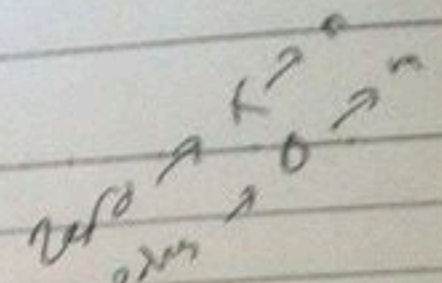




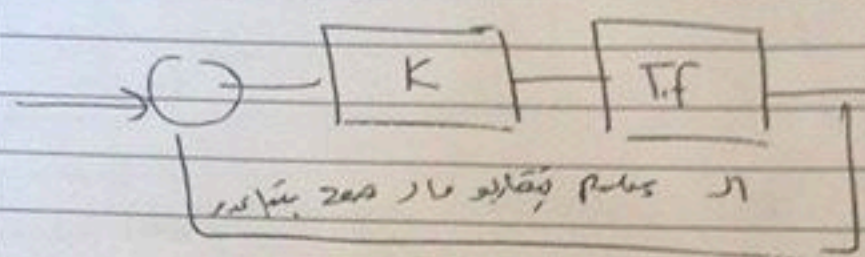
root locus (matlab)

$$G = \frac{K}{s^2 + 3s + 2} = \frac{K}{(s+2)(s+1)}$$

(stable) مابى زىقلا، كى



open loop gain  
stability  
steady state value



closed loop

تغيير  
تغيير  
gain

$$D(s) = s^2 + 3s + (2+K)$$

$$\phi = \frac{2K+1}{n-m} \text{ deg}$$

gain  
تغيير  
deg

ال pole بوقلو مار zero بوقلو

$$\sigma = \frac{\sum p_i - \sum z_i}{n-m}$$

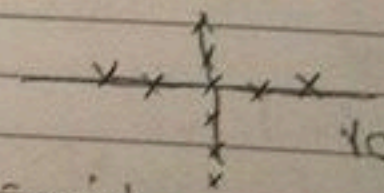
DS بوقلو مار DS بوقلو مار

$$D(s) = s^2 + 3s + (2+K)$$

DS بوقلو مار DS بوقلو مار

$$D(s) = s^2 + 3s + (2+K)$$

conjugate



root locus

$$s_{1,2} = \frac{-3 \pm \sqrt{9 - 4(2+K)}}{2}$$

$$|KG(s)| = 1$$

$$\angle KG(s) = \pi, 2\pi$$

$$\phi = \frac{2K+1}{n-m} \text{ deg}, K > 0, \Rightarrow \phi = 2K+1$$



~~$G_1 = \frac{1}{s^2 + 3s + 2}$~~

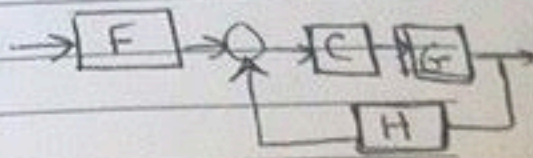
$G_1 = \frac{1}{s^2 + 3s + 2}$   
rltool

plot

Window  
Splane

PID

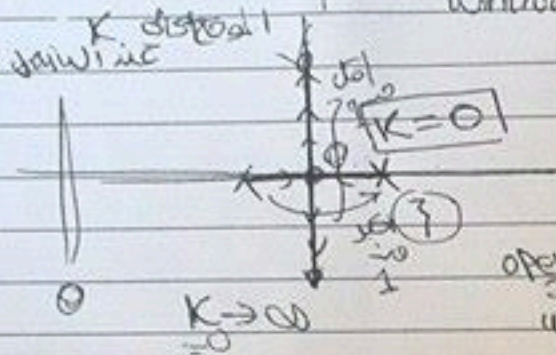
Controller



GUI =>

File -> Import -> G ->  $G_1$

under damped window



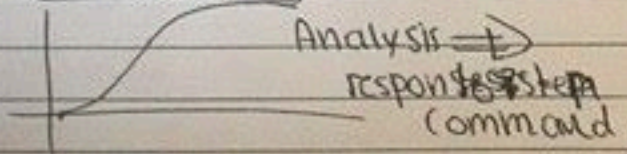
Poles -> x  
Zeros -> o

open loop poles (i)  
zeros when  $K=0$

second order system

second order system

overdamped  
 $K=0$



open loop poles ->  $K=0$   
zeros poles  $|sub>1| > 1$

underdamped (Req)



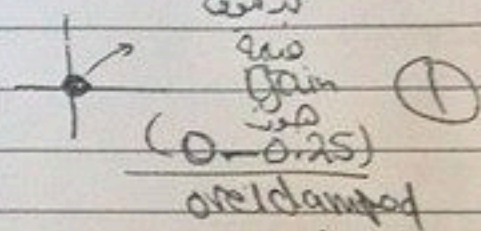
هل يمكن ان يكون النظام مستقرًا؟  
بشروط

- ① stable or not
- ② if we change the gain could be unstable?
- ③

critically damped      overdamped      under  
Real      real      imaginary  
left

critically

كيف يتغير  
مع K



0.25 is critical ②

0.25 is underdamped. ③

critically damped

3 Hz order

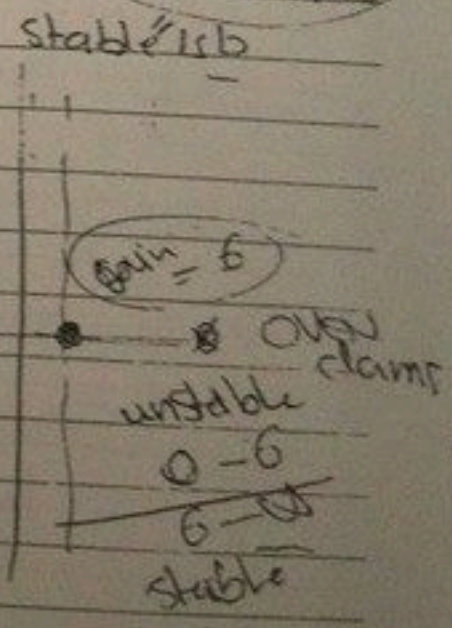
$g_1 = tf(1, [1 \ 2 \ 3])$   
File import g

under damped  
start 36  
on real axis

$g_3 = tf(1, [1 \ 1 \ -6])$

$g_4 = tf(1, [1, -6, 5])$

unstable  
K  
ماتفرقة شوفا كانت

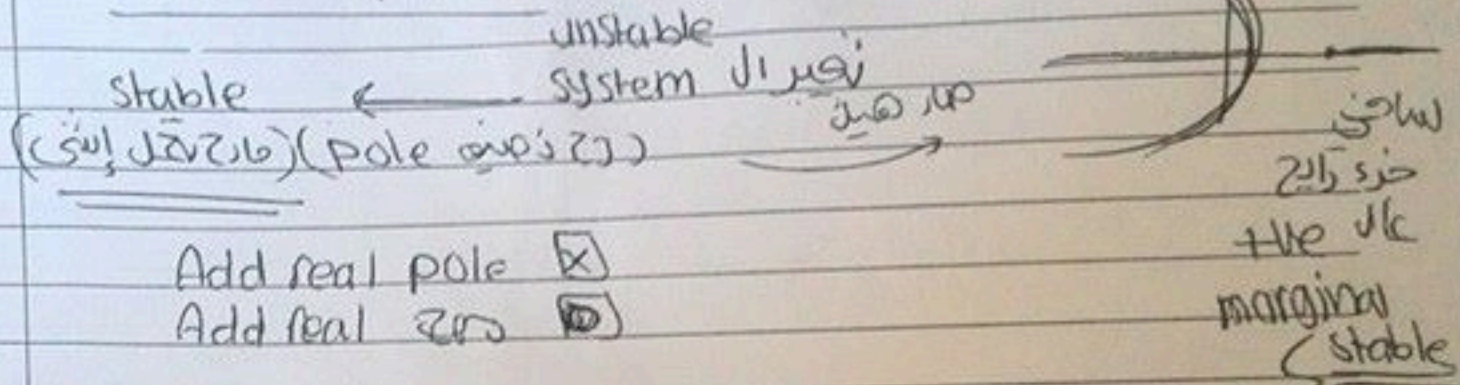




PID  $P \rightarrow$  pure  $K_p$   
 $I \rightarrow K_I \frac{1}{s}$  (integrator)  $\rightarrow$  Pole  
 $D \rightarrow K_D s$  (differentiator)  $\rightarrow$  Zero

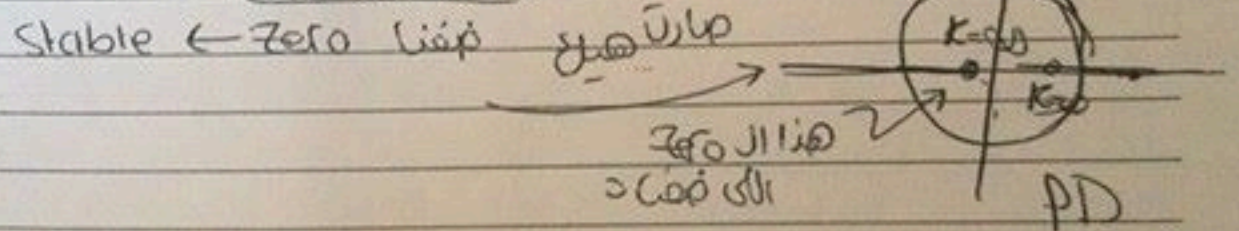
$K_p + \frac{K_I}{s} + K_D s$

PI PD



- Add real pole
- Add real zero

$\frac{Zeros}{Poles}$

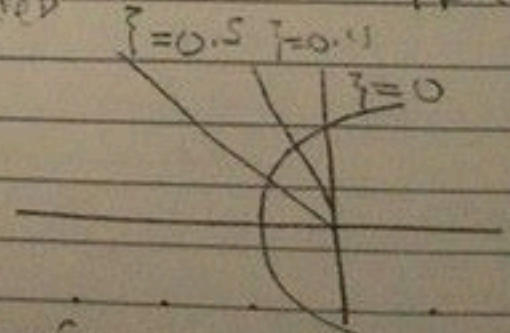


Pole-zero cancellation  
 Pole  $\rightarrow$  zero  $\rightarrow$  zero

controller form

Real  $\frac{-z \pm \sqrt{z^2 - 4p}}$  Imaginary  $\pm j \sqrt{1 - \zeta^2}$   
 $\zeta = 1$   $\zeta = 0$   
 under under  
 $\omega_n = \sqrt{(\text{Im}g)^2 + (\text{Real})^2}$   
 $\omega_n = \omega_n$   
 $\zeta = \cos^{-1} \beta$

$\frac{A + Bs}{F + Ds}$   
 PD controller



اذا طلبت من الماتلاب رسم اقطبي يسوي على اقطبي رسمت



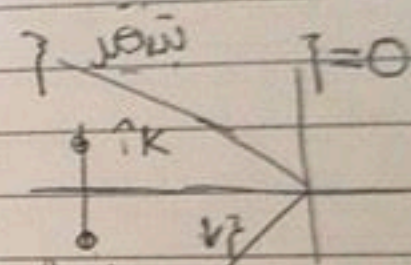
تصميم أنظمة التحكم (الجزء الأول)  
 المكان المطلوب في دائرة (دائرة)

- ① Right click on S-plane  $\Rightarrow$
- ② design requirement  $\rightarrow$  new
- ③ Range  $\zeta$  و  $\omega_n$

④ OP  $\rightarrow$  نقطة

⑤  $\zeta$   $\omega_n$   $\rightarrow$   $\zeta$   $\omega_n$

بعض المتطلبات  $\zeta$   $\omega_n$   $\rightarrow$  root locus



$\zeta \uparrow$ ,  $K \downarrow$

نقطة gain

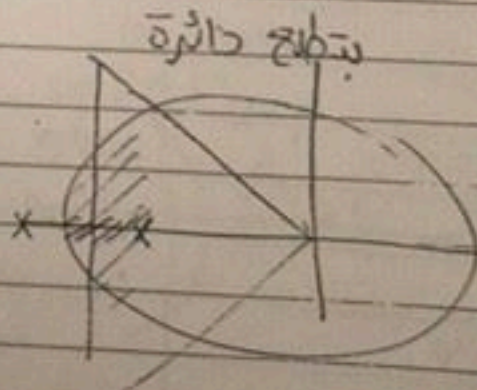
natural freq  $\omega_n$

تفسير  $\omega_n$

$\zeta > 0.4$   
 $\omega_n > 1.7$

$\omega_n < 1.7$

$\omega_n < 1.7$



المنطقة

المنطقة