



تقدم لجنة EICoM الاكاديمية

تلخيص لمختبر:

مختبر الات وقيادة كهربائية

جزيل الشكر للطالبة:

سارة أبو سارة



Drive Lab. Summary

Exp(1) Basic Measurements

theoretical part \Rightarrow

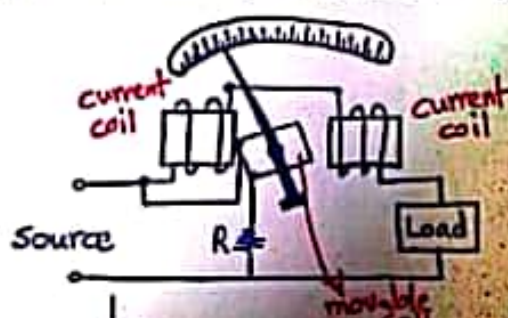
- DMM "digital multimeter", to measure ^{electrical} quantities such as (U, I, R, P) and show these values digitally.
- Voltmeter, it has a large internal resistance which is considered as an open CCT during calculations, connecting in parallel with the electrical/electronic component(s).
- Ammeter, it has a small internal resistance acting as a short CCT during calcul connecting it in series with the electrical component.
- Wattmeter, electrodynamic device consists of \Rightarrow
 - ① pair of fixed coil (current coil) which they connected in series with the CCT Load, and they're made up of few turns of a comparatively large conductance.
 - ② movable coil (potential coil) which is connected across the line and consists of many turns of fine wires.

It's mounted on a shaft, carried in jeweled bearings, so that it may turn inside the stationary coils. It carries a needle which moves over a suitably marked scale, which holds to the zero position by spiral coil springs.

When (line current) flows through the current coil, ^{عندما يمر التيار في} wattmeter ^{كيف يستطيع؟}
 a field is setup around the coil
 وقوة المجال المغناطيسي الناتج تتناسب طرديًا مع التيار، الما،
 and in phase with it.

بال (potential coil) ببيجوريس (قاومة عالية جدًا) فيتصل بالسيركس [meter] ^{متر}
 \rightarrow (purely resistive), so the current in it in phase with line voltage.

actuating force \leftarrow تنشأ ^{من} [movable coil] ^{وال} ^{الناتج} ^{المغناطيسي} ^{الناتج} ^{من} ^{التيار} ^{الخطي}
 which proportional to the instantaneous values of line current and voltage.



Three phase power system and PF :-

- 1 ϕ generator \equiv an ac generator that's designed to develop a signal sinusoidal voltage for each rotation of the shaft (rotor).
- polyphase generator \equiv develops more than one ac phase voltage per rotor rotation.

1 ϕ \rightarrow used in most small emergency generators (gasoline type)
2 ϕ \rightarrow used in servomechanisms
3 ϕ \rightarrow used by almost all commercial electric generators

1 ϕ 2 ϕ 3 ϕ

Why 3 ϕ system is preferred over 1 ϕ systems for power transmission?!

- ① Thinner conductors can be used to transmit the same kVA at the same voltage because the current is divided among the 3 phases instead of between just one, and this reduces the copper required (25% less) so that reduces also construction and maintenance costs.
- ② The lighter lines are easier to install and the supporting structure can be less massive and farther apart.
- ③ Large motors are 3 ϕ because they're self starting and don't require a special design or additional starting circuitry.
- ④ Easier motor wiring that doesn't require brushes, start capacitors, or any of the complexities of 1 ϕ motors, and are easy to reverse as needed;
- ⑤ Constant power delivery, the 3 ϕ each time a phase crosses zero there's still power being delivered, and this leads to 3 ϕ motors in machinery running more smoothly.

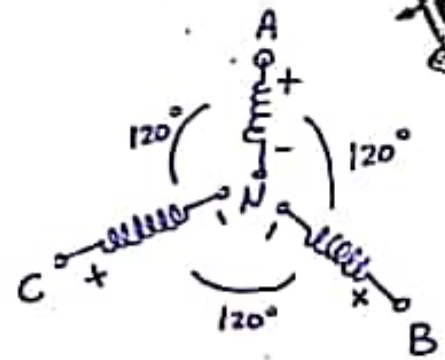
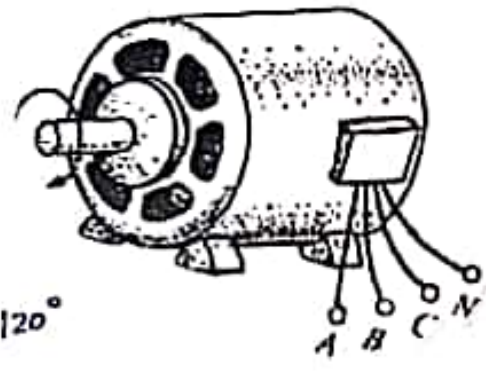
- The frequency generated is determined by \rightarrow shaft speed \cdot
 \rightarrow motor no. of poles

- $F_{\text{Jordan Europe}} = 50 \text{ Hz}$
- $F_{\text{US}} = 60 \text{ Hz}$
- $F_{\text{ships aircraft}} = 400 \text{ Hz}$

$$n = \frac{120 f}{P}$$

[rpm] P

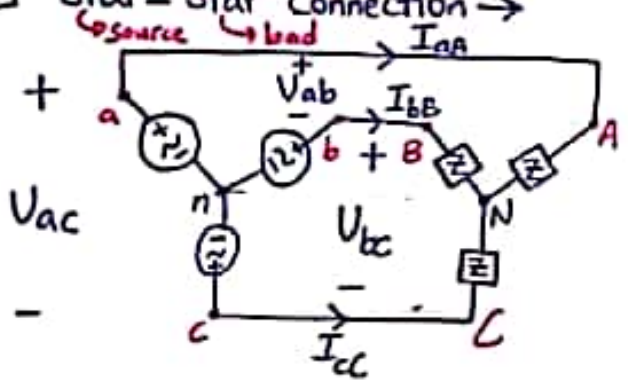
- 3 ϕ generators \rightarrow



\therefore $e_{AN} = E_{mN} \angle 0^\circ$ \leftarrow phasor form
 $e_{BN} = E_{mN} \angle -120^\circ$
 $e_{CN} = E_{mN} \angle -240^\circ$

Combination of sources and loads :-

1) Star-Star Connection \rightarrow

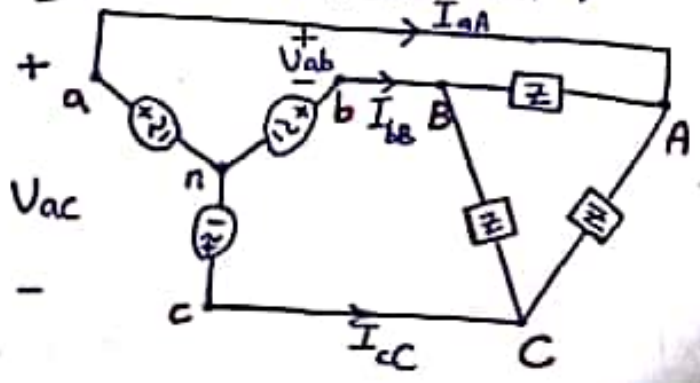


$$U_L = \sqrt{3} U_p$$

$$I_L = I_p$$

$\cdot U_L$ lead U_p by 30°

2) Star-Delta Connection \rightarrow



$$V_L = V_p$$

$$I_L = \sqrt{3} I_p$$

$\cdot I_p$ lead I_L by 30°

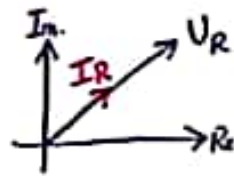
الى صوبها بالتصغير
 فيكون شوك
 السورن تكون
 عالته

- Loads $\begin{cases} \rightarrow \text{resistive} \\ \rightarrow \text{Capacitive} \\ \rightarrow \text{inductive} \end{cases}$

or combination of them

Resistive : I in phase with U

$$\boxed{PF = 1}$$



Inductive : I lagg U by 90°

$$\boxed{PF = \phi}$$

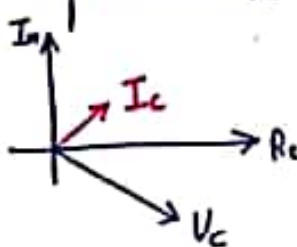
lagging



Capacitive : I lead U by 90°

$$\boxed{PF = \phi}$$

leading



- 3 ϕ power calculations :

AC power flow has three components

القدرة الفعلية

Real power (active) [W]

(P) consumed as heat losses

القدرة غير الفعالة

Reactive power (Q) [VAR]

absorbed by inductive loads or generated by capacitive loads.

القدرة الظاهرة

Apparent power (S) [VA]

$$\Rightarrow \theta = \tan^{-1} \frac{Q}{P}$$

$$\boxed{PF = \cos \theta}$$

\Rightarrow The power supplied to or drawn by a 1 ϕ is : $P_\phi = V_\phi I_\phi \cos \theta$

$$\boxed{\begin{aligned} P_{tot} &= 3U_\phi I_\phi \cos \theta \\ &= \sqrt{3} U_L I_L \cos \theta \end{aligned}} \rightarrow \text{by } 3\phi$$

- Voltage Regulation \rightarrow فرق الجهد بين الفولتية الفعالة من التوربينات بدون حمل عن V_L أو V_2 عند $R_{internal}$ بدون V_{drop} ..
the percentage of voltage difference between no load & full load voltages of a source with respect to its full voltage load.

$$\% UR = \frac{V_2(\text{no load}) - V_2(\text{with load})}{V_2(\text{with load})} \times 100$$

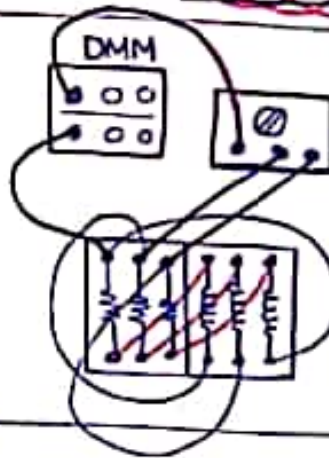
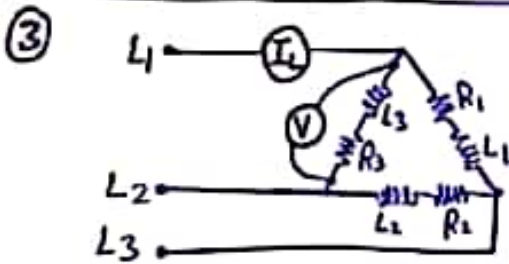
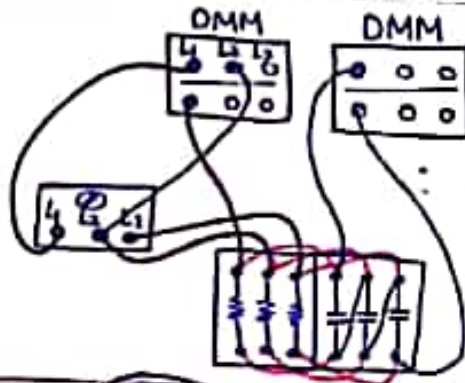
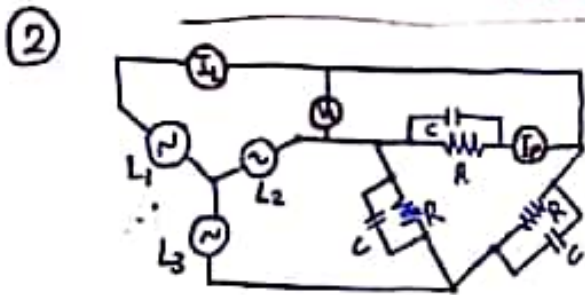
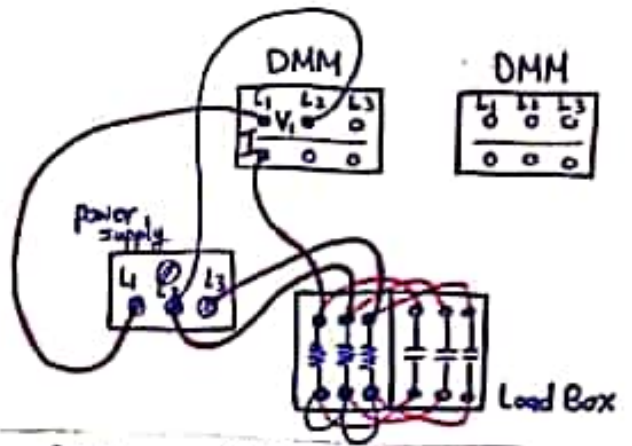
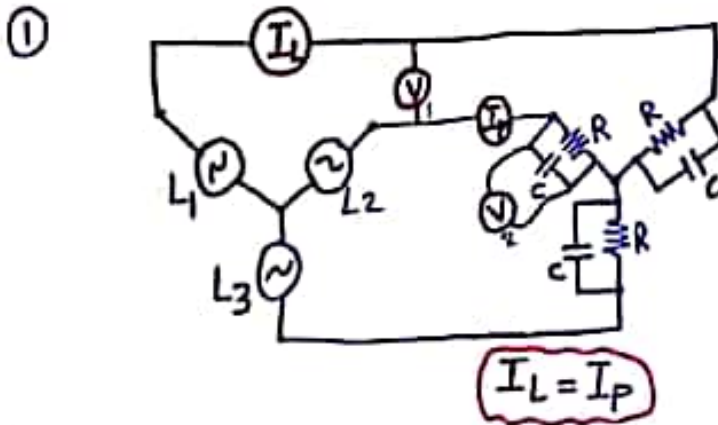
- it can be measured by $\begin{cases} \rightarrow \text{fixing the load, changing } (V_{source}) \text{ using autotransformer} \\ \rightarrow \text{fixing the supply voltage} \end{cases}$

ولقيس عنها الفولتية من ماله
ل (no load) لقيس الجهد عند الحمل
ولقيس الجهد عند ال (full load)

Practical part ⇒

Connect the circuits shown below :

بوصف الأمتار أول سويًا
لعين القولمتر



Quiz (1)

Q1) Based on the table, answer the following :

$V_L = 219.2V$	$I_L = 3.01A$	
$V_P = 218.2V$	$I_P = 2.3A$	$P_P = 121.4W$

فنأجربو فنستج انه
التشبيكة على ال
delta

1. What's the total real power?

$$P_{tot} = 3 * P_P = 3(121.4) = 364.2W$$

2. If the load connected in star instead of delta, what's the value of total real power will be? $364.2W$ (مقدري ما صحت)

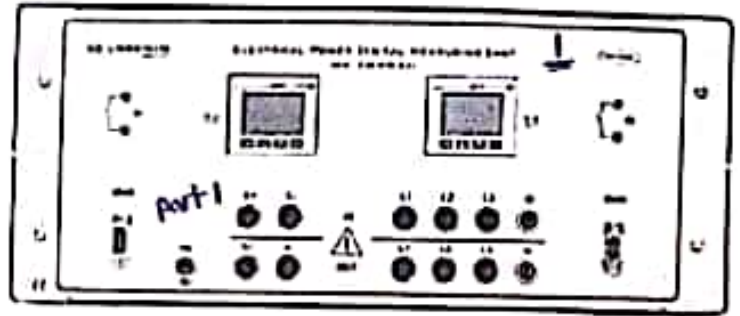
3. If the V_L without load equal $220V$, find the voltage regulation?

$$UR(\%) = \frac{220 - 219.2}{219.2} * 100 = 0.36\%$$

Q2) جاوبوا عن السؤال (units) مطلوبوا منا ...

a. What's the purpose of unit (1)?
 → (DMM) to measure electrical quantities such as U, I, P, PF, ...

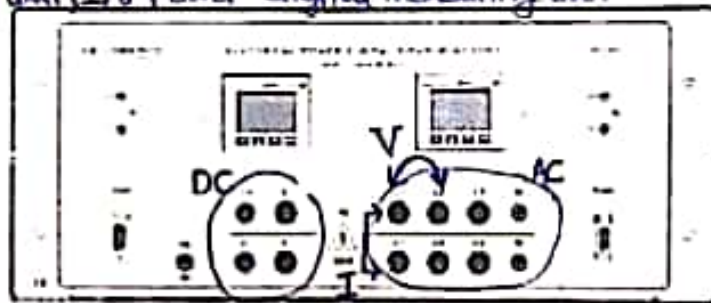
b. Can I use unit 2, part 1 to measure the phase voltage. Explain?
 → No, because it's for dc voltage measurement
 so it'll give us a zero reading in the AC measurement.



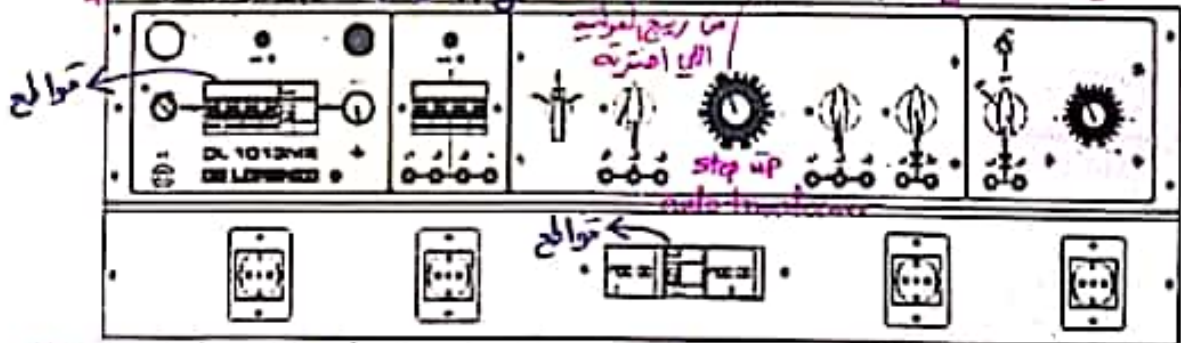
Notes :

Apparatus:

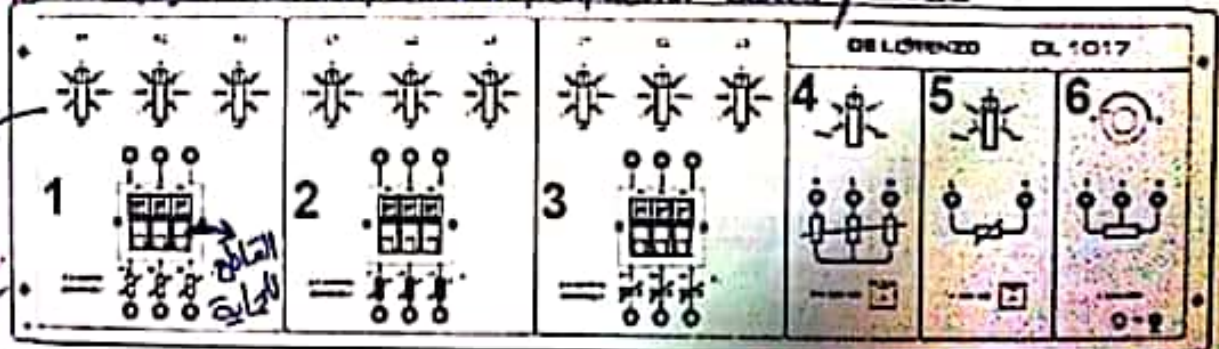
unit (1) : Power digital measuring unit



unit (2) : Power supply



unit (3) : Resistor, Inductor, capacitor boxes / Loads



تواليات
 1 max.
 7 min.
 ركون مع جفت
 الكور

Figure 1.1: System Apparatus

Exp(2) Transformers

- It's an electrical device that transfers electrical energy between two or more circuits through electromagnetic induction, that produces an electromotive force within a conductor, which is exposed to time varying magnetic fields.

بمسوقه للزيادة أو للتقليل من الـ (alternating voltages) في electric power application

- Varying current in the transformer's primary winding creates a varying magnetic flux in the transformer core, and a varying field on the transformer's secondary winding which induces a varying emf due to electromagnetic induction.

Transformer's Core and shell forms →

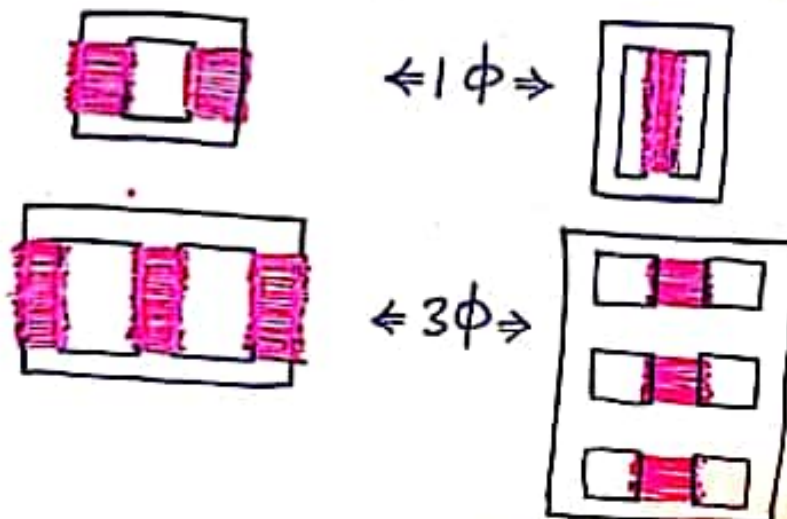
Closed core transformers are constructed in 2

① Core form →
windings surround the core

② Shell form →
windings surrounded by the core

- more economical for high voltage power transformer applications at the lower end of their voltage and power rating ranges (≤ 230 kV or 75 MVA)

- more prevalent for transformer distribution applications due to the relative ease in stacking the core around winding coils.
- They're characterized as having better kVA to weight ratio, better short cct strength characteristics and higher immunity to transit damage.



Transformer Tests →

An important point is to define the transformer's low voltage side and high voltage side.

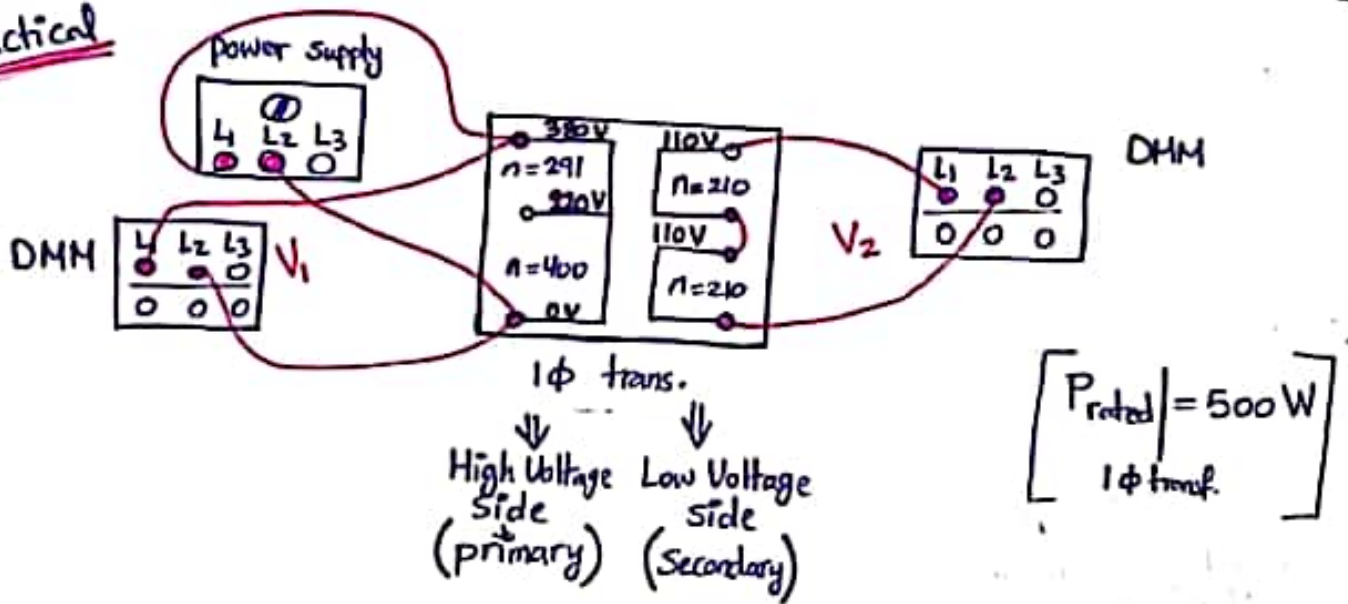
↳ Turns ratio test: at no load

تطبيق فولتية صغيرة على ال (primary) وقياس بالفولتميتر الفولتية الخارجة من ال (secondary)

$$a = \frac{V_P}{V_S} = \frac{I_S}{I_P}$$

↳ for ideal transformers „no losses“

practical



* ويمكن أضيف لعدد مع ملفات ال (secondary) وأقصى V_2 يوجد لها ويطلق ال UR

Notes :

بال (1 φ transf.) ← PE ⊙ العبود فيه فستقره لتفريغ أسلاك

والكهرباء الساكنة من على جسم المحول في اعتبار انه فستقله بشكل

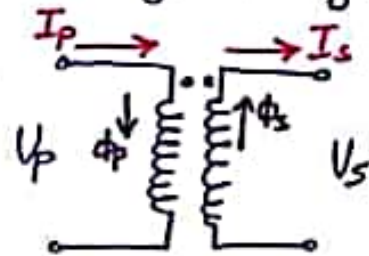
سريع ولتفريغ طويلة...
 فيه ما فستقره باللا لأنه ما فستقله المحول بالتمية الكبيرة التي علينا نتابعه

• إما يستعمل (V_{S1}) and/or (V_{S2}) ، (V_{P1}) or (V_{P2})

2.] Windings polarity test (Dot Convention):

- Voltage polarities are the same with respect to the dots on each side of the core.
- If the current flows to the dotted end of the primary, the I_s will flow out of the dotted end of the secondary winding.

because when I_p induce Φ_p in a certain direction, the secondary coil will induce Φ_s that will oppose the Φ_p in direction.

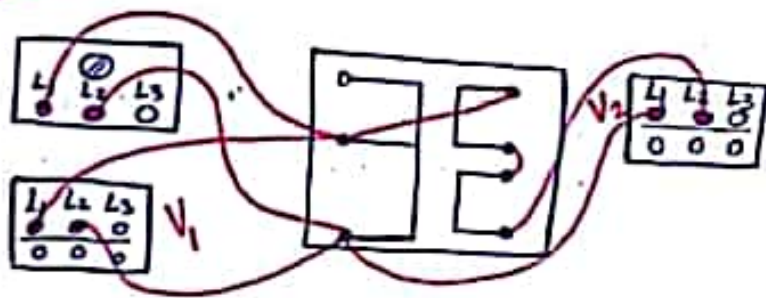


IMP

Importance of polarity test

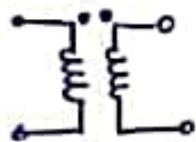
→ to know the relative polarities at any instant of the primary and the secondary terminals for making the correct connections if the transformers are to be connected in parallel or they're used in a 3 ϕ circuit.

practical



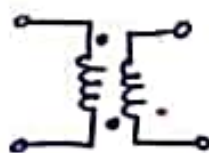
بطبق فولتية على ال primary (V_1)
ويجعل شوية بسلك بين واحد من
أطراف ال primary مع واحد من أطراف
ال secondary
ويقيس الفولتية التي بتطلع من ال
unshorted terminals
(V_2)

* if $V_1 > V_2$, subtractive



→ the transformer voltage are in phase

if $V_1 < V_2$, additive



→ the transformer voltages are out of phase

3] Load Test : (supply voltage) البيكون ال primary سبوك مع secondary سبوك على ال واللود بيكون سبوك على ال ويعين الغولية الحالة ويعايرها بيون اللود الاصيب (UR)

- The with-load (η_{actual}) \rightarrow $\eta_{\text{actual}} (\%) = \frac{P_{\text{out}}}{P_{\text{in}}} * 100$
 - $P_{\text{out}} = I_2 V_2$ (for a purely resistive load)
 - $P_{\text{in}} = P_{\text{out}} + P_{\text{cu}} + P_{\text{iron}}$

(η_{max}) occurs when $[P_{\text{cu}} = P_{\text{iron}}]$

- Because a real transformer has series impedance within it, the output voltage from it varies with load even if the input voltage remains constant.

$$UR(\%) = \frac{U_2(\text{no load}) - U_2(\text{with load})}{U_2(\text{with load})} * 100$$

secondary voltage

سنا على
تسبب الجهد وغرنا
اللود مع تيار
(R_{prot})

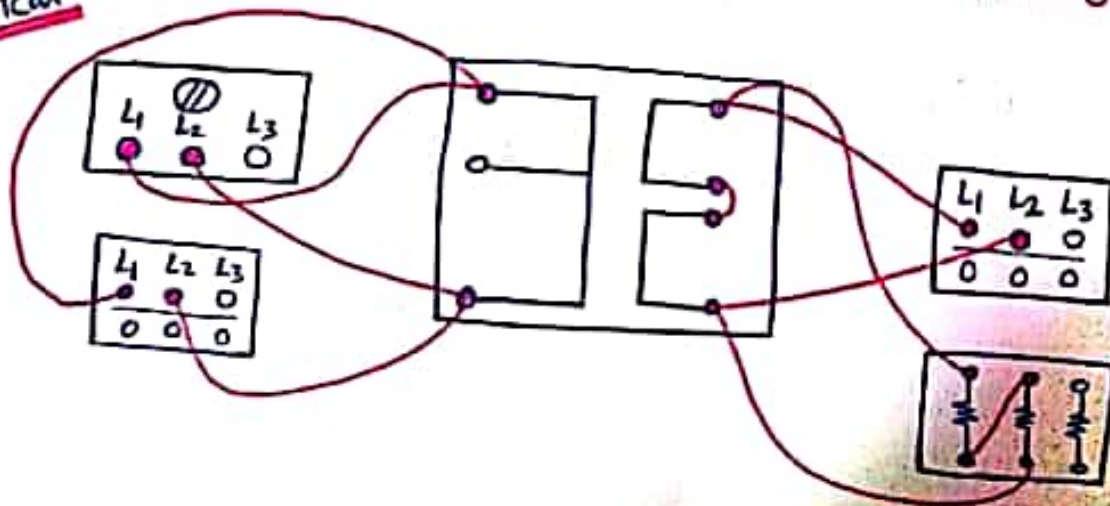
To protect the transformer, (R_{prot}) added in series with the (load) with a min. value \rightarrow to prevent ($I_{\text{secondary}}$) to exceed its rated value.

$$I_{\text{rated}} = \frac{P_{\text{rated}}}{V_{\text{rated}}} = \frac{500 \text{ W}}{320 \text{ or } 220} \text{ [A]}$$

$$R_{\text{min}} = \frac{V_{\text{rated}}}{I_{\text{rated}}} \text{ [\Omega]}$$

ص
سوال الغولية الي
أضربها في ال
primary

Practical



4) Three phase connection : (Star/Delta)

• Star Connection →

advantages

- a. allows the 4 wire distribution
- b. allows the phases to be insulated for a voltage 1.73 times less than the line voltage
- c. star centre can be connected to earth and this stabilizes the voltage value.

disadvantages

- a. When used on the primary, it doesn't allow the free flowing of the 3rd harmonic
- b. this rise to deformation of the flux waves and the phase voltages

• Delta Connection →

advantages

- a. When used on the primary, it imposes the values of the phase voltage under any load condition, therefore ensuring the voltage symmetry
- b. allows the free flowing of the 3rd harmonic
- c. doesn't introduce any deformation of the fluxes and the voltages.
- d. When used on the secondary, it damps 3rd harmonic of the fluxes leaving the induced currents free to flow
- e. it allows the reduction of the winding sections, which are sized for a current 1.73 times smaller.

disadvantages

- a. it doesn't allow 4 wire distribution (in the output side)
- b. it doesn't allow the earth connection
- c. so, in case of the earth fault, could be even stressed by the whole line voltage

* the most suitable connections are → primary (delta)

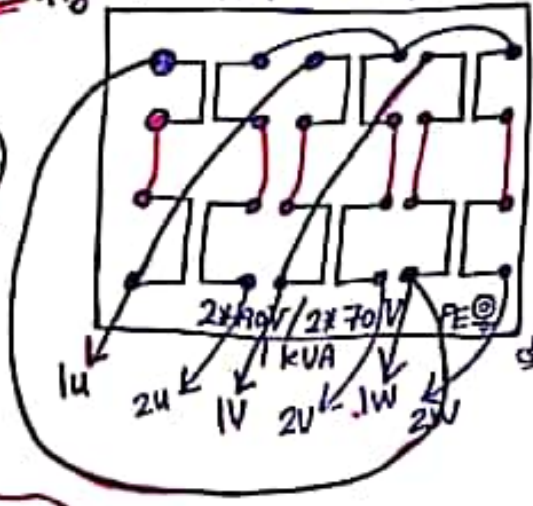
secondary (star)

في حالة كنا جاهة كل المنتر

أو الكاب الأرضي

فإننا ذلك نعتبرها على ذلك

practical Fig(1) 3 ϕ transf.



أصين
لوجين

$V_p = 190V$
 $V_s = 70V$

Series delta/ Series star

primary secondary

Rated line voltage \rightarrow

$V_{HV} = 2 \times 190V = 380V$ (delta: $V_L = V_p$)

الخطان
التي فوقها
تحت

$V_{LV} = \sqrt{3} \times (2 \times 70) = 245.5V$ (star: $V_L = \sqrt{3} V_p$)

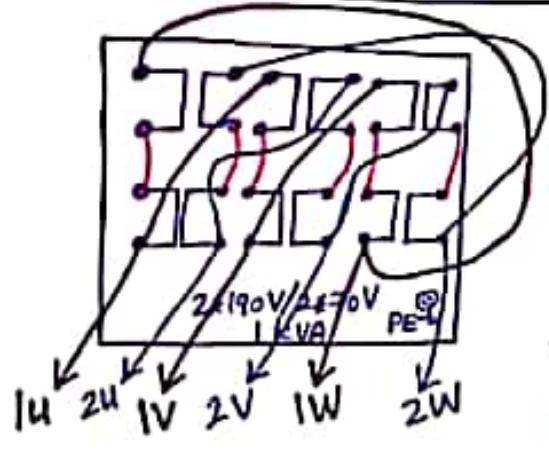
Rated line current \rightarrow

$I_{HV} = \sqrt{3} \times \frac{1000VA}{3 \times (2 \times 190)} = 1.52A$ (delta: $I_L = \sqrt{3} I_p$)

لاي حستين ال 3 لابلان
التي تحتها

$I_{LV} = \frac{1000VA}{3 \times (2 \times 70)} = 2.38A$ (star: $I_L = I_p$)

Fig(2)



Series delta/ Series delta

Rated line voltage \rightarrow

$V_{HV} = 2 \times 190V = 380V$

$V_{LV} = 2 \times 70V = 140V$

Rated line current \rightarrow

$I_{HV} = \sqrt{3} \times \frac{1000VA}{3 \times (2 \times 190)} = 1.52A$

$I_{LV} = \sqrt{3} \times \frac{1000VA}{3 \times (2 \times 70)} = 4.12A$

Discussion & Analysis Questions

- Q1) Does the transformer voltage ratio stay the same when a load is applied? Why?
 \rightarrow No, due to the drop voltage occurs on the internal impedences of the primary & secondary that increases due to loading current (I^2R) so V_2 drops at the same V_1
- Q2) Why does the wattmeter in the no load test read the iron core losses only?
 \rightarrow because the voltage in it's approximate the rated. So, the iron losses that depends on the voltage across the windings, is considerable.

$P_{iron} = I^2R$

Exp(3) Shunt DC Motors

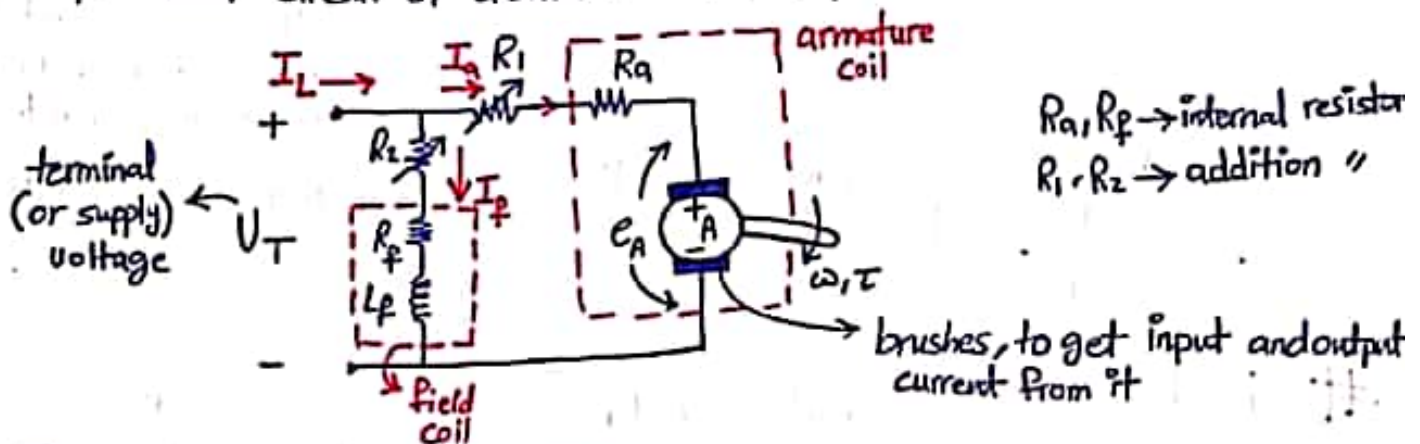
Theoretical part \Rightarrow

بیشتر از کبیر ال [Separately Excited DC Motor] لکن الفرق هو:

- SEDM \rightarrow has its field CCT connected to an indep. Voltage supply
- SDM \rightarrow has its field CCT connected across the armature motor terminals.

وعلى ذنن انه ال supply voltage ثابت فان مبدأ عمل كلا منها يكون نفس الشيء.

Equivalent Circuit of a shunt DC Motor \rightarrow



if $[R_1 = R_2 = \emptyset] \rightarrow U_T = e_a + I_a R_a$ where $\begin{cases} \tau = k\phi I_a \\ e_a = k\phi \omega \\ I_L = I_a + I_f \end{cases}$

$$= k\phi \omega + \frac{\tau}{k\phi} R_a$$

$$\omega = \frac{U_T}{k\phi} - \frac{R_a}{(k\phi)^2} \tau \rightarrow (\tau - \omega) \text{ relation}$$

* How does a shunt dc motor respond to a load ?

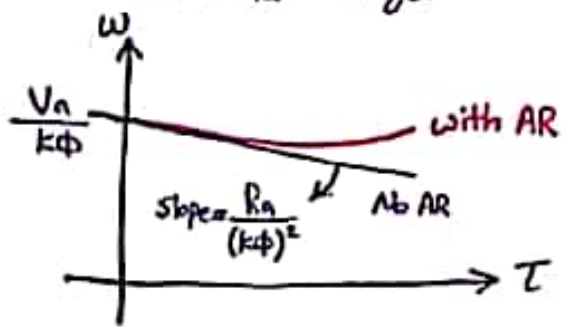
increasing the load that's connected to the motor shaft, will cause increasing in the (τ_{load}) exceed the (τ_{ind}) in the machine, so the motor starts to slow down.

ولا سرعة الموتور بتبليغ تعلق \leftarrow the internal generated voltage $(E_A \downarrow)$

$\left[\downarrow E_A = k\phi \omega \downarrow \right]$ so the $(I_a \uparrow)$ $\left[I_a \uparrow = \frac{U_T - E_A \downarrow}{R_a} \right]$ and then $(\tau_{ind} \uparrow)$ $\left[\tau_{ind} = k\phi I_a \right]$

until it equals to the τ_{load} at a lower mechanical speed of rotation.

← فن تلك علاقة $(\tau - \omega)$ السابقة، حيث تتغير سرعة الموتور بشكل خطي مع التورق
 لنفترض كل المتغيرات الأخرى في العلاقة تظل ثابتة (R_a, ϕ, I_a)
 as load changes



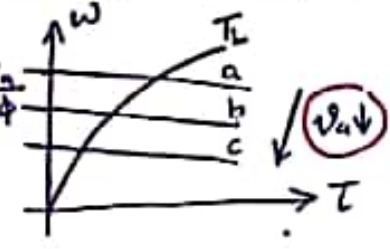
$(\tau - \omega)$ characteristics curve

- Linear relation with a negative slope
- مشكلة بتأثير شكل المغنيس نتيجة
 as the load increases, the flux weakening effect occur and that causes the speed to increase over the speed at no AR at any given load.

← الحل هي إضافة اللفظ في الموتور التي تجعل ϕ يبقى ثابتاً.
 فنقدر نثبت السرعة على أي قيمة من التورق طالما يعرف مقدار I_a

Speed Control of a shunt DC motor → للتحكم في سرعة موتوري الشنت (3 طرق)

1) Armature Voltage :
 للسرعات الأقل من (ω_{base})
 requires variable DC supply

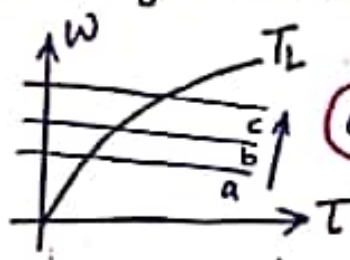


← مع نقصان V_a
 تنقل ال ω
 تنقل ال τ

advantages → doesn't change speed regulation
 → speed is controlled from $[\phi - \omega_{base}]$

disadvantages → cost is higher because of using power electronic controllers

2) Field Flux :
 للسرعات الأعلى من (ω_{base})
 by changing R_f



← مع نقصان ϕ
 يزيد ω
 يزيد τ

غير مناسبة
 PHDC Permanent magnet DC motor

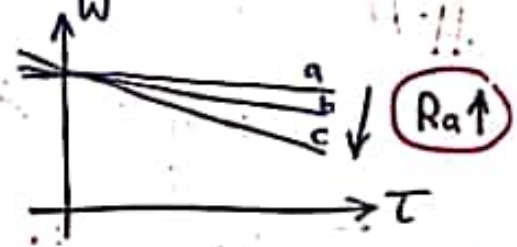
advantages → speed control above base
 → the cost of rheostat is small because it has small value.

disadvantages → speed regulation is poor
 → At high speeds flux is small thus causes the speed to become unstable

3] Armature Resistance (R_a):

موصوفة كـ كثيرهاى الطريقة

because it reduces the motor efficiency due to the losses



↑ R_a \leftarrow زيادة
↑ slope \leftarrow يزيد
↓ ω \leftarrow تنقص

advantages

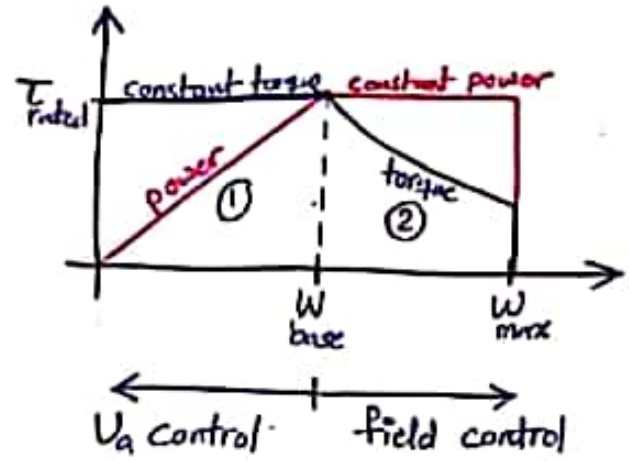
- starting and speed control combined in one rheostat
- the speed range begins at zero speed
- cost is less for the same speed range than other methods
- Simple method

disadvantages

- Introduce losses in rheostat thus low η
- Speed regulation is poor

Motor characteristics →

أي قيمة التورق يكون أعلى من ال (rated) will cause the shaft to stop "get locked"



$$\omega_{max} = 30\% \omega_{rated}$$

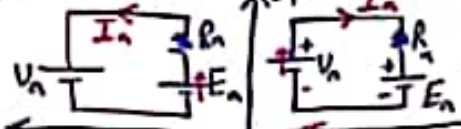
- In region (1) : (T_{rated}) ويكون عندك (U_a) ويكون الود ثابتة U_a يطبق (U_a) ويمكن تطبيقه على المحرك الذي يمكنه ان يدير حتى ω_{base} that can be applied to the shaft that can run at speeds up to the ω_{base}
- In region (2) : مع زيادة السرعة لازم يعاينها نقصان الود المحرك مع ال (shaft) لأنه اذا زاد الود مع السرعة فيزداد التورق وبالتالي فيزيد سحب التيار الذي ينتج من زيادة الفولتية المطلوبة ولكنها بالأساس سغلة U_a فقط على ال rated value للاريا فقط.

Modes of Operation → SEDM

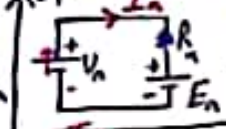
السعة فيها بين القطبين كما هي

ليس هي نفسها الـ Shunt

Forward braking ($E_n > U_n$)
انكسرت التوليد بنفس اتجاه التوليد

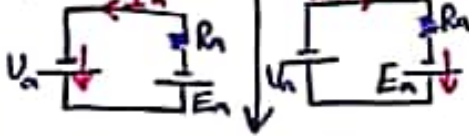


forward motoring ($U_n > E_n$)



Torque

Reverse motoring ($|U_n| > |E_n|$)



Reverse braking ($|E_n| > |U_n|$)

Practical part ⇒

Nameplate:

DE LURENZO

20 viale Ramagnan - 20089 ROVATO (VI) ITALY

Generator Code

Type of machine

supply voltage

Nominal power (P_{out})

Insulation class

Constructive norms

serial no.	51 0000 00
armature current *	rated armature current I_a
	rated output power P_{out}
	rated (base) speed ω_{base}
field current *	rated field current I_f
	rated field voltage
Degree of Protection	SHUNT

serial no.

armature current *

field current *

عداد التوليد
السعة عن غيره انه
في قيمتين للتيار
a → f

$I_a > I_f$

* القيم على الـ (name plate) عبارة عن قيم تشغيلية لكن الـ [max values] يكون أكبر منها → 30%

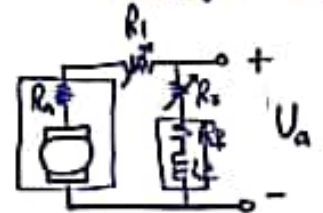
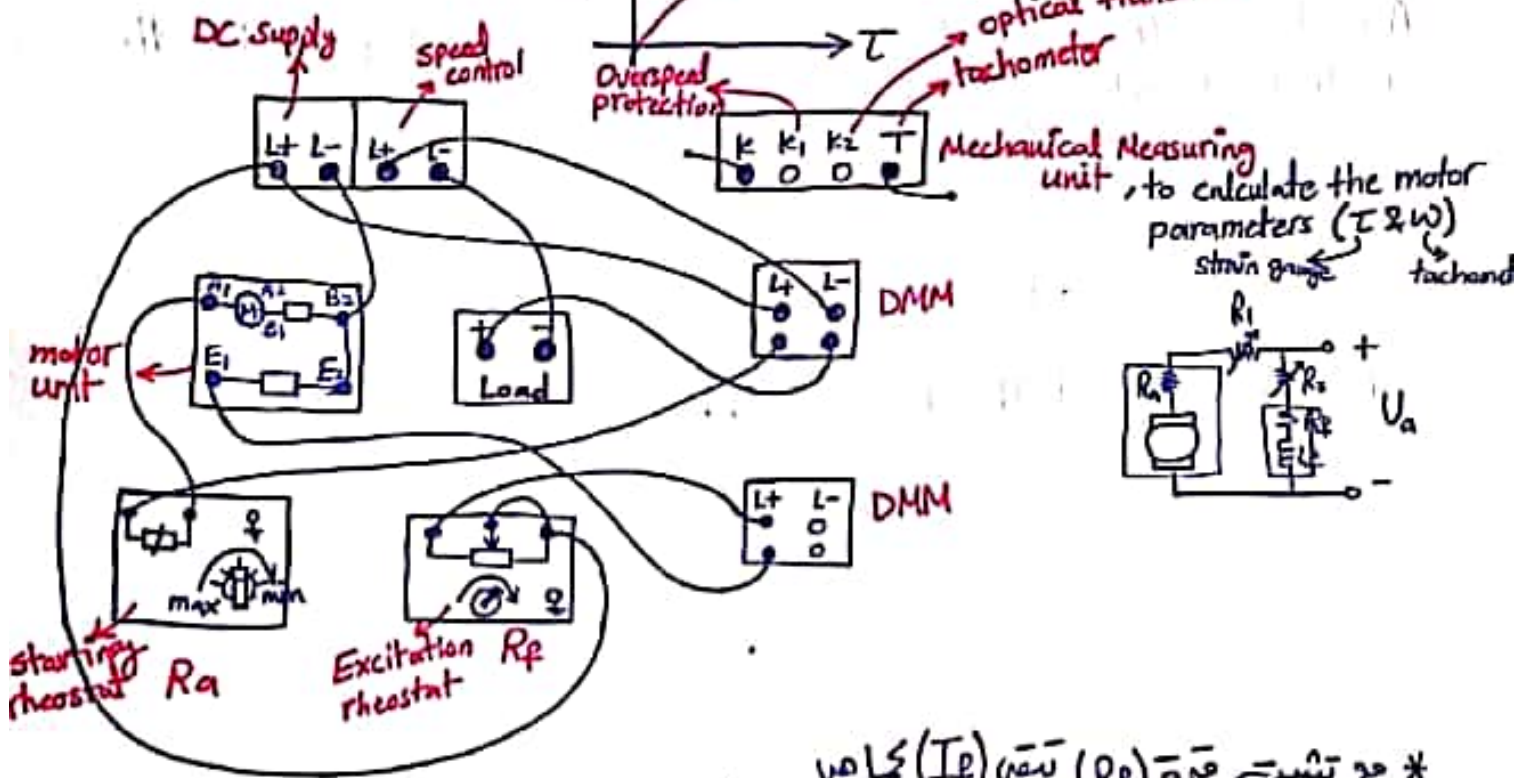
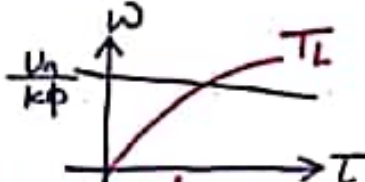
$$P_{in} = U_T (I_a + I_f)$$

$$P_{out} = \frac{2\pi n T}{60}$$

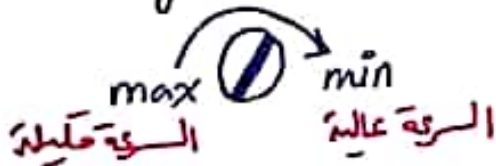
$$T_{rated} = \frac{P_{rated (out)}}{\omega_{rated (base)}}$$

In this Lab, we'll be looking at the properties of the shunt by increasing the load using an electromagnetic brake to achieve pre-specified currents. load

① (T-W) Curve →



* starting Rheostat (Ra) :-

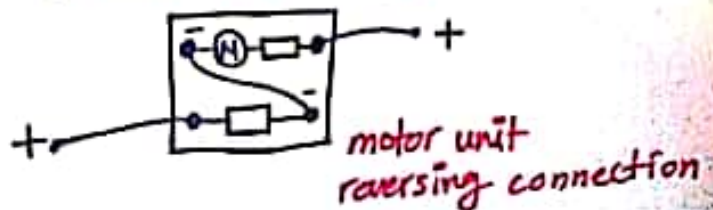


used for starting & speed control.

② Altering (Rf) → بزَيَاة Rf أَسْرَدَاد ω

③ Altering (Va) → بزَيَاة Va أَسْرَدَاد ω

④ Reversal of shunt direction → بَعْسَ قَطْبِيَّةِ ال (armature) أَوِ ال (field) عَكْسَةَ قَطْبِيَّةِ ال (armature) هَوَ



* مع تَبْيِيَةِ قِيَمَةِ (Rf) بِنَقْصِ (If) كَمَا فِي

بَزِيَاةِ اللُّوْدِ تَقَلُّ السَّرْعَةُ، تَبْقَلُ E_a

بِزِيَادِ I_a وَالتَّوَلُّدِ T

Quiz Questions

- I can increase the flux of a shunt DC motor by dec. the field resistance.
- Main difference between speed control by voltage and field flux control in dc motors is the voltage to control speeds below the base & field flux for above the base
- According to the terminal characteristics of the shunt DC motor, the method of control in the following fig. is U_T



- Increasing U_T of the shunt will not change the load torque.

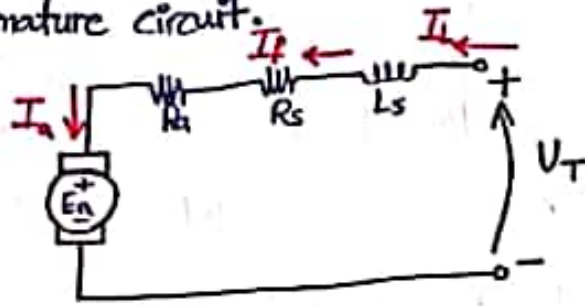
Exp (4) Series DC Motor

theoretical part \Rightarrow

- It's a motor whose field windings consists of a relatively few turns connected in series with the armature circuit.

$$I_A = I_f = I_L$$

$$V_T = E_a + I_a (R_a + R_s)$$



- The basic behaviour of a series DC motor, due to the fact that $\phi \propto I_a$, at least until saturation is reached.

$$\phi = c I_a$$

\leftarrow مع زيادة اللود يزداد ϕ فيتبدل السرعة

$$\begin{aligned} \tau_{ind} &= k \phi I_a \\ &= k c I_a^2 \end{aligned}$$

$$\tau_{ind} = k I_a^2$$

وهذا الذي يميز موتور ال series عن ال shunt انه يبسط τ_{ind} على ليربطه بسيم استخدام الموتور

starter motor in cars \leftarrow
elevator motors \leftarrow

tractor motors in locomotives \leftarrow

The terminal characteristics of a series dc motor \Rightarrow

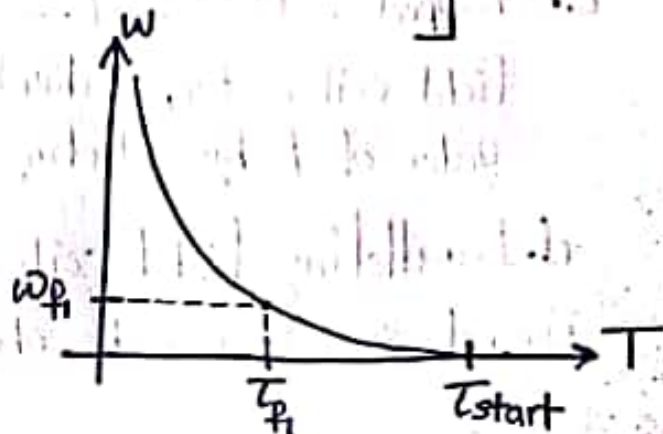
$$V_T = E_a + I_a (R_a + R_s)$$

$$I_a = \sqrt{\frac{\tau_{ind}}{k c}}$$

$$E_a = k \phi \omega$$

$$\Rightarrow \left[V_T = k \phi \omega + \sqrt{\frac{\tau_{ind}}{k c}} (R_a + R_s) \right]$$

$$\omega = \frac{V_T}{k c \sqrt{\tau_{ind}}} - \frac{R_a + R_s}{k c}$$



Series DC Motor Disadvantage

→ When the motor torque goes to ϕ , the speed will go to ∞ . In practice, due to the mechanical, stray and core losses the torque can never be zero.

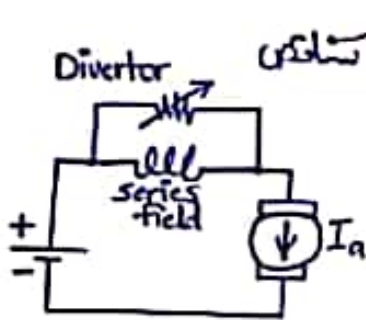
If no other load connected to the motor, it can turn the motor fast enough to damage itself.

يعني أبداً حابيه أعلاه unloaded على الموتور وهو مشغول

Speed Control of series DC motor

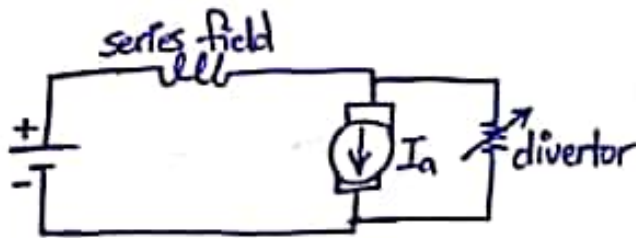
1 Flux Control :

a. Field diverter → بإضافة مقاومة مقابله (R_{div}) على التوازي مع (R_p) بتقليل التيار (I_a) وبالتالي بتقليل ϕ فبتزيد السرعة.



لكن مع استمرار الزيادة على قيمة (R_{div}) تنمير السرعة تستلزم لقيمتها السابقة.

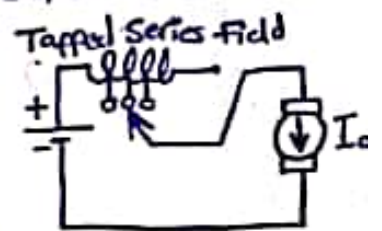
b. Armature diverter → For a given constant load (torque)



التيار (I_a) يبقى ϕ يزداد فيتقلد (السرعة)

c. Tapped field control →

field coil is tapped dividing no. of turns. Thus, we can select different value of ϕ by selecting different no. of turns.



d. Paralleling field coils →

Several speeds can be obtained by regrouping coils.



3] Variable Resistance In Series with Armature →
 إضافة مقاومة على التوالي مع R_a في (U_n) وتقل السرعة

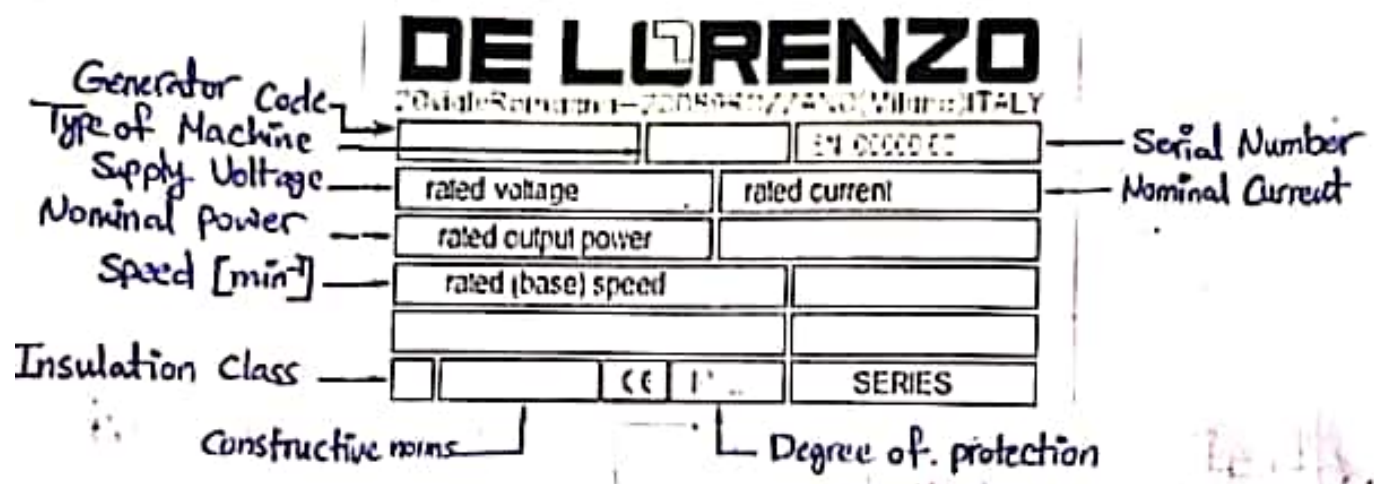
3] Varying (U_n) →

إذا تقل ال armature voltage تقل السرعة معها والتعكس $U_n \propto \omega$

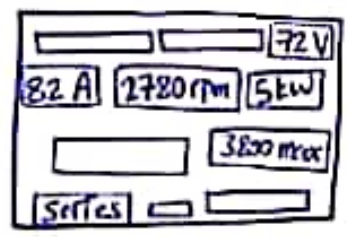
• Differences between shunt and series motors →

- 1 Series should be loaded all the time
- 2 Torque in the series much higher than the T_{ind} in the shunt
- 3 Cross sectional area of series > cross sectional area of a shunt
- 4 Series no. of turns < shunt no. of turns

Series dc motor nameplate :-



Q_{mid}



① Find T_{rated} ? $T_{rated} = \frac{P_{rated}}{\omega_{rated}} = \frac{5 \text{ kW}}{\frac{2\pi}{60} (2780)} = 17.17$

② Find $(k\phi)$ at the T_{rated} ? $T_{rated} = (k\phi) \cdot I_a$
 $17.17 = (k\phi) \cdot 82$
 $k\phi = 0.209$

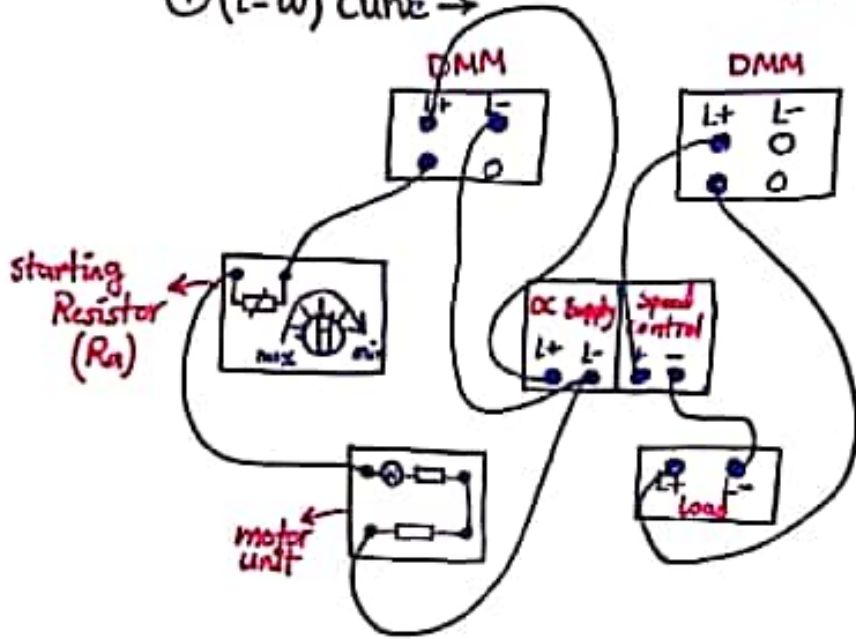
③ Find R_{total} assume no losses (mechanical)?

④ Find E_a assume no mechanical losses?

practical part \Rightarrow

ذاتياً عند تشغيل اللود انه سيحس عند ال starting
بعدمه لود ما بصير نستبح ابرم

① (T-W) Curve \rightarrow

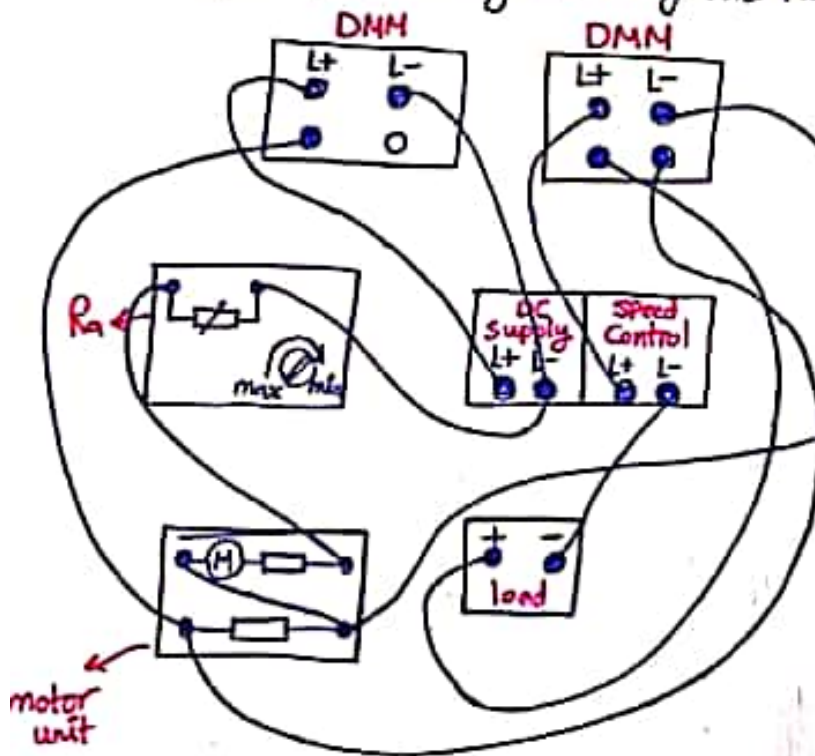


* تيار البدن والغولبية المصنعة
عالم ال series أعلى من ال shunt
* مع نقصان $R_{a\text{net}}$ ، تزداد ω
* عند زيادة اللود يتقل ω
 \rightarrow $(\uparrow T, \uparrow I_a, \phi, I_f)$

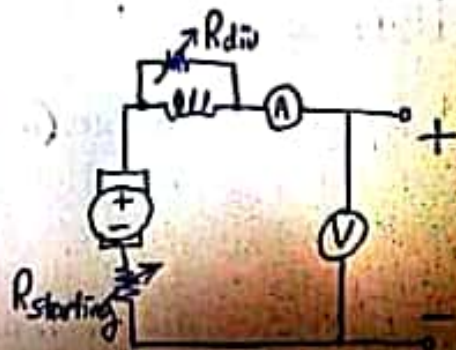
② Speed control by changing (V_T) \rightarrow

بزيادة V_T تيزداد معها السرعة والحكم

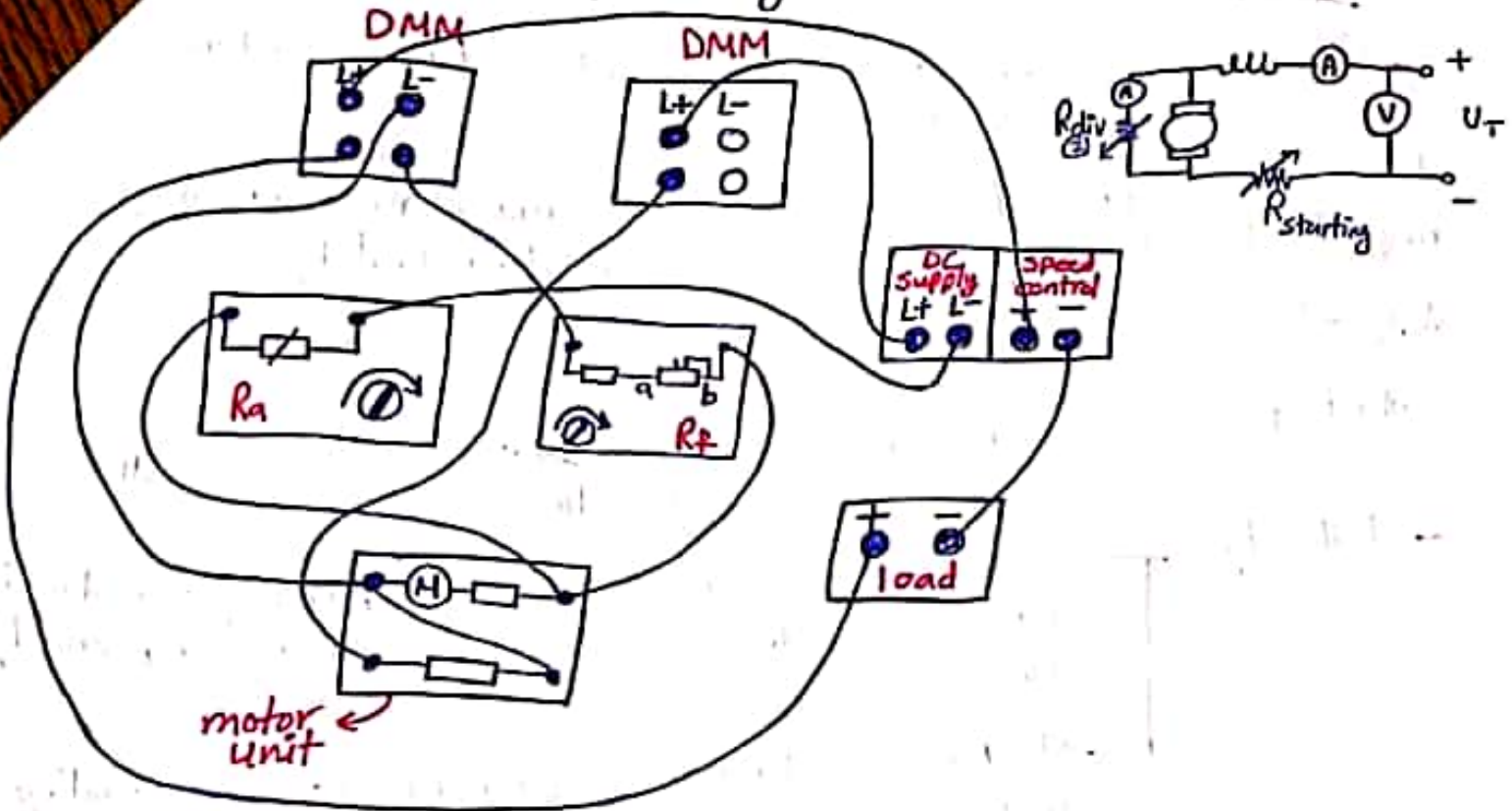
③ Speed control by shunting the field CCT \rightarrow



بغيره اللود عشان I_a
رإف ما بصير عليها سي
(بغيره ال field من ال diverter)
والعلاقة عكسية
بين ω مع R_{div}



(4) Speed control by shunting the armature circuit →



For a given T_L , if ($I_a \downarrow$) then ($\phi \uparrow$), as $[T_a \propto I_a]$, this will increase the current taken from supply ($I_T \uparrow$), ($\phi \uparrow$), ($\omega \downarrow$)

Quiz Questions

- The 2 ways of changing the I_a during series experiment are divertors & load.
- Increasing the flux in the series will _____ the I_a
- What is the flux control methods can be applied in our lab? divertors
- During this experiment, which resistor we used in start control?
Starting Rheostat (R_a)
- State 2 methods of starting control in series dc motor?

Exp (5) Three Phase Induction Motors

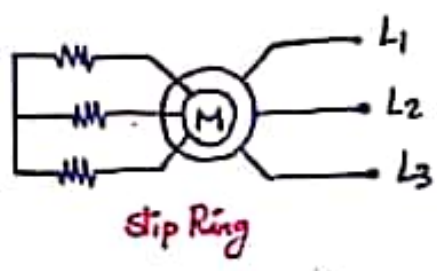
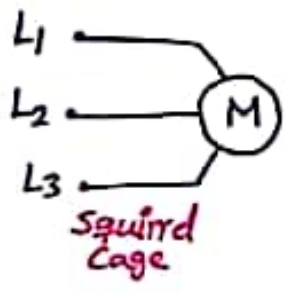
- It consists of $\begin{cases} \rightarrow \text{Stator, connected to a 3}\phi \text{ power system} \\ \rightarrow \text{Rotor} \end{cases}$

due to the 120° phase shift between each successive phases, a rotating magnetic field is produced in speed that can be determined by:

وبالتالي سرعة المجال المغناطيسي $\rightarrow n_{sync} = \frac{120f}{P}$

which passes over the rotor bars and induces a voltage in them
 ولها السبب صغيره induction motor.

- Rotor type \rightarrow Squirrel cage, consists of a series of conducting bars laid in slots carved in the rotor face and shorted at either end by large shorting rings
- \rightarrow Slip Ring "Wound Rotor", has a complete set of 3 ϕ windings that are mirror images of the stator windings. Extra (R) can be added.



The Concept of Rotor Slip \rightarrow

- The voltage induced in a rotor bar of an induction motor depends on the speed of the rotor relative to the magnetic fields.

$$n_{slip} = n_{sync} - n_m \rightarrow \text{rotor speed}$$

\swarrow
stator speed

if $n_m = n_{sync} \rightarrow \text{slip} = 0$
 $n_m = 0 \rightarrow \text{slip} = 1$

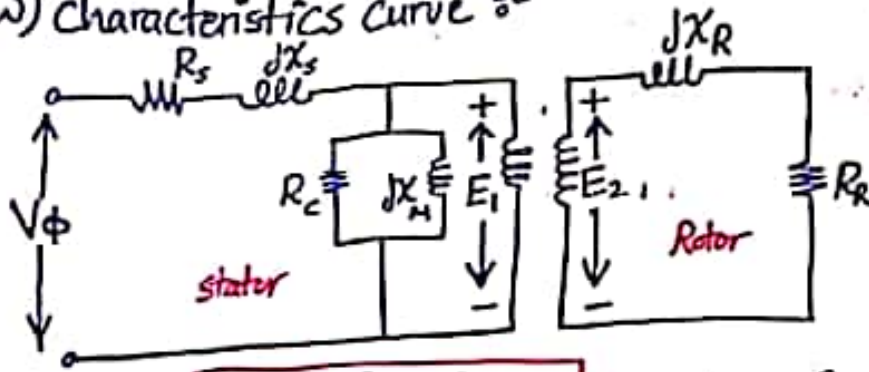
$$n_m = (1-s)n_{sync}$$

$$\text{Slip} = \frac{n_{slip}}{n_{sync}} \times 100\%$$

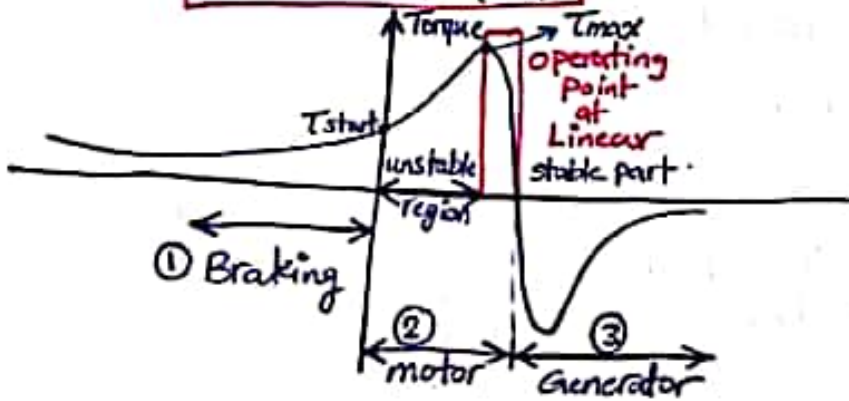
- Induction motor works by inducing voltages and currents in the machine rotor
- If the rotor is locked, so it will have the same frequency as the stator

$$f_{rotor} = s f_{stator}$$

(T-w) characteristics curve



$$T = k_s E_2^2 \frac{R_2}{\sqrt{R_2^2 + (sX_2)^2}} \quad \text{where } k = \frac{3}{2\pi n_{\text{stp}}}$$



Operating Regions

① Braking → $n_m < 0$ • torque is (+ve) while speed is (-ve)
 "plugging" slip > 1

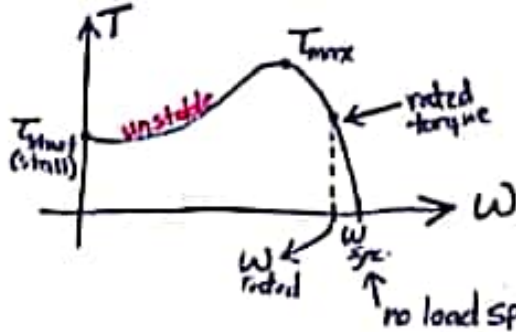
this mode of operation can be used to quickly stop a machine, by switching two phases which causes the result of changing the direction of motion of the stator magnetic field.

② Motoring → $0 < n_m < n_{\text{sync}}$ • torque and motion are in the same direction
 $0 < \text{slip} < 1$

the most common mode of operation.

③ Generating → $n_m > n_{\text{sync}}$ • torque is (+ve) while speed is (-ve)
 slip < 0

Unlike plugging, if the power converted is (-ve), so is the air gap power.



- at no load, the IM operates at ω_{sync}
- as the load increases (due to bearing & load friction), the machine slows down
- If the motor is overloaded, it will reach to the max. torque

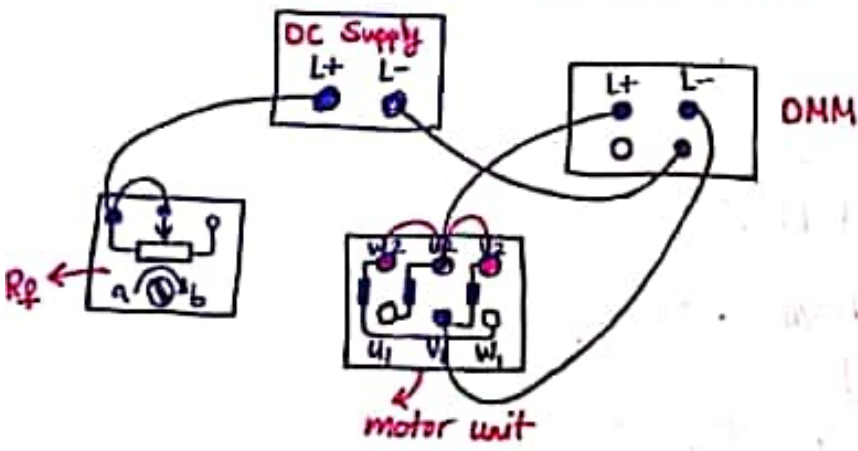
Practical part ⇒ **باللآب استخرنا (Squirrel cage) طابع منه ٣ حالات**

Three tests are used to determine the parameters of the induction motor model:

1) DC test: بتطبيق (dc voltage) على الـ stator ويزيد منه حتى يتر الـ (I_{rated}) بدون حاسباته
 by applying a variable dc voltage to two terminals of the stator winding that should be increased so that the current flowing in the stator winding reaches the rated current.

$$R_s|_{\Delta} = \frac{3}{2} \frac{U_{DC}}{I_{DC}} \leftarrow \begin{matrix} U_{rated} \\ I_{rated} \end{matrix} \leftarrow \text{مقدار تيار قوة (R_s)}$$

$$R_s|_{\text{star}} = \frac{1}{2} \frac{U_{DC}}{I_{DC}}$$

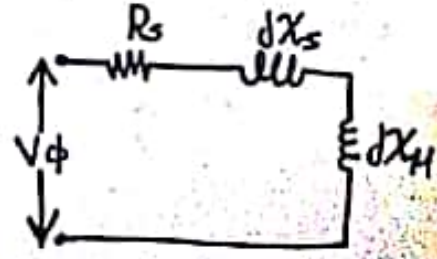


2) No Load test: This test is carried out with a delta connected stator. during this test, IM operates as motor and run at ω_{sync} (slip $\rightarrow 0$). Therefore, all P_{in} will be consumed as losses: stator copper losses ($I_{\phi}^2 R_s$) core losses & mechanical rotational losses (friction and windage losses).

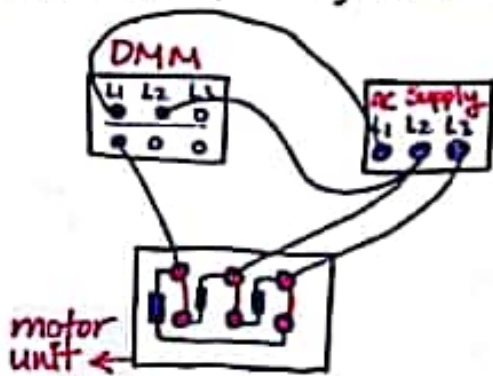
$$P_{rot} = P_{in, NL} - P_{Cu, s}$$

$$= P_{in, NL} - 3I_{\phi}^2 R_s$$

$$X_M = \frac{V_{\phi}}{I_{\phi}} \sin \theta - X_s$$



Connecting the motor (stator) in delta :

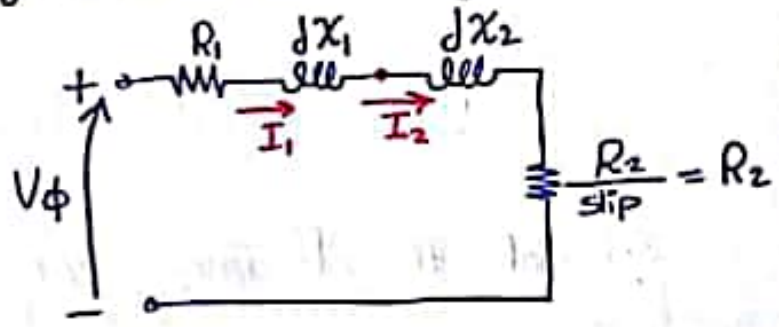
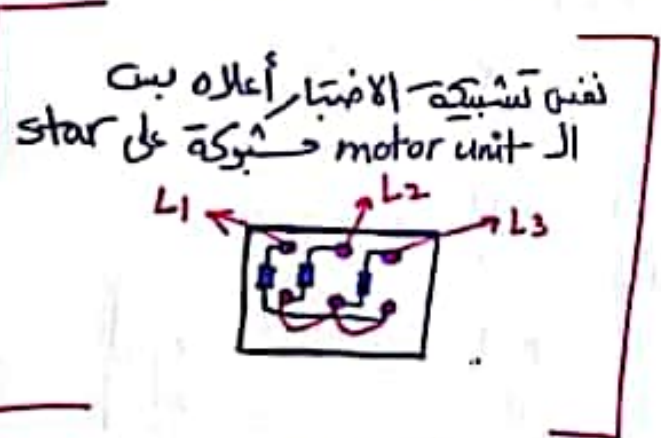


3] Locked Rotor Test :

by applying low voltage on the stator terminals (motor unit) so that the rotor doesn't rotate and its speed becomes zero and full load current passes through the stator winding.

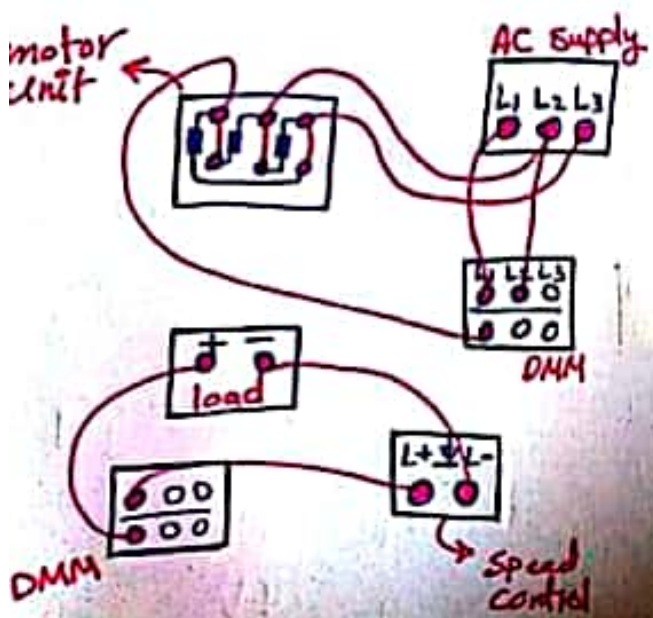
لو كنت الفولتية المطبقة عالية فالسنت قد تتسبب في إتلاف ملفات الـ Stator

then, slowly increasing the voltage in the stator winding so that current reaches to its rated value.



4] Load Test : to study (τ-w) curve of the IM and its efficiency

بنتي نفس الفولتية بالمبة (220V) مثلا
 لنوجد للـ rated ، بقدر على اللود τ_{load}
 ولتسوف شو بصير على السرعة



مقياس سرعة الدوران

3φ induction motor nameplate :

DE LORENZO	
<small>POVLE RARAGNA - 330890077 AND MIERO ITALY</small>	
Generator Code	3~M
Type of machine	SI: 000000
Supply voltage	220/380 V Δ/Y
Nominal power	1.1 kW
speed	2870 min ⁻¹
	4.3/2.5 A Δ/Y
	cos φ = 0.8
	50 Hz
	CE I ..

Q1 From the above nameplate, answer the following : [If the motor have 2poles] rated slip = 0.05

1.) Calculate the synchronous speed ? $n_{sync} = \frac{120f}{P}$

$$= \frac{120(50)}{2} = 3000$$

2.) Calculate the input power ? $P_{in} = \sqrt{3} V_L I_L \cos \theta$

$$= \sqrt{3} (220)(4.3)(0.8)$$

$$= 1311 \text{ W}$$

ولو أضفنا قيم $I_L = 2.5 \text{ A}$ و $V_L = 380 \text{ V}$ ← صيغ نفس الجواب تقريباً

3.) Calc. the efficiency ? $\% \eta = \frac{P_{out}}{P_{in}} = \frac{1100}{1311} \times 100$

$$= 83.9\%$$

4) Calculate the motor speed (n_m) ? (mechanical)

$$n_{slip} = n_{syn} - n_m$$

$$slip = \frac{n_{slip}}{n_{syn}} \Rightarrow n_{slip} = (0.05)(3000) = 150 \text{ [rpm]}$$

$$\therefore n_m = n_{syn} - n_{slip}$$

$$= 3000 - 150$$

$$= 2850 \text{ [rpm]}$$

#

Q2 For the no load test, $R_s = 8.5 \Omega$

V_{L-L}	I_L	P_{tot}	N_m [rpm]
220 V	2.45A	152W	2989

Find P_{tot} ?

$$\begin{aligned} P_{tot} &= P_{nl} - 3I_{\phi}^2 R_s \\ &= 152 - 3 \frac{(2.45)^2}{(\sqrt{3})^2} (8.5) \\ &= 100.98 \text{ W} \quad \# \end{aligned}$$